

Spin-boson description of electron transmission through a molecular wire [☆]

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1. Introduction

Originally, the spin-boson model has been introduced as a generic description of particle or quasi-particle transfer in two-level systems coupled to a dissipative environment with the latter described as huge set of independent harmonic oscillators [1–4]. This model attracted particular interest when studying the driving by external regular and stochastic fields [5–8]. However, the outstanding importance of the spin-boson model is mainly related to the fact that a large variety of results do exist. A generalization of the spin-boson model to multi-level systems can be found at different places (cf., e.g. [6,9,10]). In the present paper, we will carry out such

a generalization to describe the inelastic charge transmission through *molecular wires* [11,12].

Intensive research work has been invested on the study of molecular wires, i.e., single molecules or polymer strands embedded in between two electrodes (for a recent reviews, see [13–21]). These diversified activities are not only caused by the fundamental interest on electron transfer (ET) processes in single molecules or solid-state molecule hybrid structures. Further motivation has also been originated by the long-standing wish to control micro-currents in molecular devices via, e.g., rectification or gating [11,12,22–28]. Recent experimental results on the conductivity of single molecules [29–34] may serve as a good starting point to clarify the physical mechanisms of such a control.

Most of the theoretical approaches on molecular wires focused on the description of an elastic current in utilizing the Landauer–Büttiker theory [35,36]. In this approach charge motion through the molecular wire is described as a multitude of elastic scattering processes [20,28,30,31,37]. If *inelastic* processes contribute to the

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overall current what will be the case whenever dephasing processes within wire units destroy the ET coherency the problem becomes more involved [14,17,38–44].

The investigation of the current–voltage (I – V) characteristics of a molecular wire combined with a study of its wire-length dependency became an important way to reveal the mechanism of charge transmission. It is well-known from studies on ET reactions in molecular complexes that fast nuclear relaxation processes result in the sequential (hopping) mechanism of ET along the molecular chain (see, e.g. [45]). In the case of a molecular wire and if a small voltage V is applied this mechanism is responsible for the Ohmic regime of ET. Now, the dependence of the wire conductance on the number of wire units N is proportional to the factor $\sim [1 + \xi(N - 1)]^{-1}$ [41]. A similar dependence (like $\sim [A + B(N - 1)]^{-1}$) has been proposed by Nitzan and co-workers [46] to fit data on the N -dependency of an overall steady-state rate constant. Moreover, Bixon and Jortner [47] used such types of expressions to describe long-range charge transfer reactions in DNA stacks.

The other basic ET mechanism may become observable in those molecular wires where the energy gaps between the wire LUMO-levels and the Fermi-levels of the electrodes are large. Now, one may state that the LUMO-levels act as virtual states only. The inter-electrode current results from a coherent tunneling process which is induced by the so-called superexchange inter-electrode coupling [13,20,28,48]. It drops exponentially ($\sim \exp[-(\xi/2)(N - 1)]$) with an increase of the number of bridge units N . As in the theory of ET reactions in molecular complexes the sequential as well as the superexchange mechanism have also to be considered as fundamental charge transfer processes in molecular wires [20,28,37,44,49].

Elastic as well as inelastic mechanisms of charge transmission through molecular wires result from a complicated interplay of dynamic and relaxation processes. For instance, the efficiency of the elastic interelectrode current strongly depends on the level-broadening of the terminal wire units. This broadening results from the coupling to the continuous conduction band spectrum of the electrodes [13,28,30,37]. Moreover, relaxation processes within each wire determine the inelastic part of the overall current [14,28,41–43]. To achieve a correct consideration of all ET mechanisms (including the formation of superexchange couplings between the electrodes and separated wire units, as well as the various dephasing processes) a unified theoretical description becomes necessary.

It is the goal of the present paper to present such a unified description of the interelectrode current mediated by a molecular wire. However, we will concentrate on the nonadiabatic regime of charge transmission [50]. Within such a regime the ET occurs against the background of fast nuclear relaxation and, thus, the molec-

ular vibrational degrees of freedom can be considered as a thermal bath. Additionally, our description focuses on a model for which the electronic energy levels of the terminal wire-units are positioned much below the electronic levels of the internal wire-units. In this case, a long-ranged superexchange ET between the terminal sites has to be considered along with the complete sequential charge transfer processes through the wire. Then, the total inelastic current is formed by a mixture of sequential and superexchange contributions.

The paper is organized as follows. Section 2 is devoted to a generalization of the spin-boson model for the description of the ET system “left electrode (L)–molecular wire–right electrode (R)” (LWR). Section 3 deals with the derivation of an analytic expression for the inelastic interelectrode current. We take a particular model for the wire where the LUMO energies of its terminal units are positioned much below the LUMO energies of the internal wire-units. In Section 4, an exact analytic form of the thermally activated current is derived. The conditions are specified at which the current is given by additive contributions from the sequential (hopping) mechanism and the superexchange mechanism (related to the superexchange coupling between the terminal wire units). Analytic and numerical results on the length-dependence of the inelastic interelectrode current are presented in Section 5. In Section 6, a general discussion can be found on the length-dependence of the wire mediated current.

2. Spin-boson model of a molecular wire

This section is devoted to a derivation of the LWR-system Hamiltonian valid for an arbitrary number of wire units. We will employ a semiphenomenological tight-binding approximation and suppose the electronic coupling among the wire units and between the wire and the electrode to be weak. The wire should be characterized by a linear arrangement of $N + 2$ units which are embedded between two nano-electrodes (cf. Fig. 1). The energy of the transferred excess electron at the m th wire unit is given by $E_m = E_m^{(0)} + \Delta E_m(V)$ where $\Delta E_m(V)$ is the shift caused by the applied voltage V . Obviously, the E_m differ from the site energy $\epsilon_m^{(0)}$ valid in the absence of the excess electron. Therefore, the energetic differences

$$\epsilon_m = E_m - \epsilon_m^{(0)} = \Delta \epsilon_m^{(0)} + \Delta E_m(V), \quad (\Delta \epsilon_m^{(0)} = E_m^{(0)} - \epsilon_m^{(0)}), \quad (1)$$

define the affinity of the m th wire unit to an extra electron and thus can be refer to LUMO-level energies.

One way to characterize the electronic levels of the LWR-system is the use of a second-quantization notation (see, e.g. [53]) based on fermionic creation (a_j^\dagger) and annihilation (a_j) operators which act on the states $|N_j\rangle$. Since the occupation numbers are $N_j = 0, 1$ the states

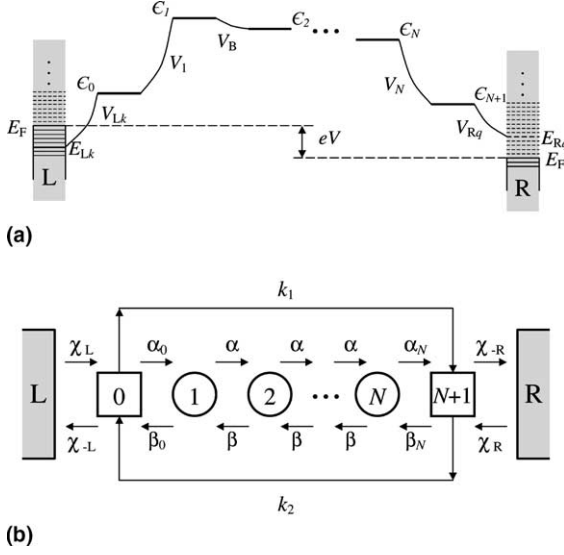


Fig. 1. Energetic (a) and kinetic scheme (b) of nonadiabatic ET through a linear molecular wire. The quantity V_{Lk} (V_{Rk}) is the coupling among the LUMO-level with energy E_0 (E_{N+1}) and the electrode level with band energy E_{Lk} (E_{Rk}). The coupling V_{Lk} (V_{Rk}) are responsible for the formation of the wire-site electrode transition rate χ_L and χ_{-L} (χ_R and χ_{-R}). The wire-site to site electronic transfer couplings $V_1 \equiv V_{10}$ ($V_N \equiv V_{NN+1}$) between the (local) LUMO-levels with energies ϵ_0 and ϵ_1 (ϵ_N and ϵ_{N+1}) form the intersite rate constants α_0 and α_1 (β_0 and β_1). Analogously, the coupling $V_B \equiv V_{mm+1}$ are responsible for the formation of wire internal interior site-site transition rates α and β .

$|0_j\rangle$ and $|1_j\rangle$ refer to the vacuum states of the excess electron and for the state of a single excess electron, respectively (for the present purposes there is no need to account for the electron spin). Note also the normalization condition

$$\sum_{N_j=0,1} |N_j\rangle\langle N_j| = 1. \quad (2)$$

For the LWR-system under consideration the index j has to be related to the states of the two electrodes ($j = Lk, Rk$, where \mathbf{k} is the wave vector of the electrode conduction band) and the local wire-unit states ($j = m = 0, 1, \dots, N+1$). Accordingly, the electronic Hamiltonian of the LWR-system can be represented in the following form:

$$H_{LWR}^{(el)} = H_{LR}^{(el)} + H_W^{(el)} + H_{LR-W}^{(el)}, \quad (3)$$

where the two electrode Hamiltonian read

$$H_{LR}^{(el)} = \sum_{s=L,R} \sum_{\mathbf{k}} E_{s\mathbf{k}} a_{s\mathbf{k}}^+ a_{s\mathbf{k}}. \quad (4)$$

The electronic part of the wire Hamiltonian follows as

$$H_W^{(el)} = \sum_{m=0}^{N+1} [E_m a_m^+ a_m + \epsilon_m^{(0)} a_m a_m^+] + \sum_{m=0}^N [V_{mm+1} a_m^+ a_{m+1} + V_{m+1m} a_{m+1}^+ a_m]. \quad (5)$$

The $V_{mm'}$ denote the intersite electronic couplings. Finally, the wire-electrode coupling Hamiltonian is taken as

$$H_{LR-W}^{(el)} = \sum_{\mathbf{k}} [V_{Lk} a_{Lk}^+ a_0 + V_{Lk}^* a_0^+ a_{Lk}] + \sum_{\mathbf{q}} [V_{Rq} a_{Rq}^+ a_{N+1} + V_{Rq}^* a_{N+1}^+ a_{Rq}], \quad (6)$$

where V_{Lk} and V_{Rq} are the couplings of the terminal wire units, 0 and $N+1$, to the left and to the right electrode, respectively. The electronic Hamiltonian, Eqs. (3)–(6) will be taken as a basic quantity for any further description. The expression has only to be completed by those contributions following from the nuclear dynamics.

To achieve a notation similar to that used for the standard spin-boson system we change to an electronic occupation number representation. An application of the rules $a_j^+ |N_j\rangle = (1 - N_j) |1 - N_j\rangle$ and $a_j |N_j\rangle = N_j |1 - N_j\rangle$ yields

$$H_W^{(el)} = \sum_{m=0}^{N+1} \sum_{N_m=0,1} [E_m N_m + \epsilon_m^{(0)} (1 - N_m)] |N_m\rangle\langle N_m| + \sum_{m=0}^N [V_{mm+1} |1_m\rangle\langle 0_m| \otimes |0_{m+1}\rangle\langle 1_{m+1}| + h.c.]. \quad (7)$$

The nuclear part of wire Hamiltonian, $H_W^{(nucl)}$, will be taken in its most simple form by providing that each vibrational frequency $\omega_{\lambda m}$ with mode index λ is independent on the presence or absence of the transferred electron at site m . [For the Holstein model [54] the vibrational frequencies become independent on the site index m as well.] Let $M_{\lambda m}$ be the effective mass corresponding to the λ th normal mode and let the quantities $-C_{\lambda m}$ and $+C_{\lambda m}$ define the vibrational equilibria at the presence or the absence of the excess electron, then we may write

$$H_W^{(nucl)} = \sum_{m=0}^{N+1} \sum_{\lambda} \left\{ \frac{p_{m\lambda}^2}{2M_{m\lambda}} + \frac{M_{m\lambda} \omega_{m\lambda}^2}{2} \left[q_{m\lambda} - (2N_m - 1) \frac{C_{m\lambda}}{M_{m\lambda} \omega_{m\lambda}^2} \right]^2 \right\} \times |N_m\rangle\langle N_m|. \quad (8)$$

Next, we introduce the vectorial operator σ_m which components are given by

$$\sigma_m^z = |1_m\rangle\langle 1_m| - |0_m\rangle\langle 0_m|, \quad (9)$$

$$\sigma_m^x = |1_m\rangle\langle 0_m| + |0_m\rangle\langle 1_m|, \quad (10)$$

$$\sigma_m^y = -i(|1_m\rangle\langle 0_m| - |0_m\rangle\langle 1_m|). \quad (11)$$

The $\sigma_m^{x,y,z}$ satisfy Pauli's commutation relations and σ_m can be referred to a local Pauli pseudo-spin operator. Noting the definitions (9)–(11) as well as the normalization condition (2) one can rewrite the wire Hamiltonian $H_W = H_W^{(el)} + H_W^{(nucl)}$ to obtain the following expression:

$$\begin{aligned}
H_W = & E_0^{(\text{el})} + E_0^{(\text{nucl})} + (1/2) \sum_{m=0}^{N+1} \left[\epsilon_m + \sum_{\lambda} \kappa_{\lambda m} (b_{\lambda m}^+ + b_{\lambda m}) \right] \sigma_m^z \\
& + \sum_{m=0}^{N+1} \sum_{\lambda} \hbar \omega_{\lambda m} (b_{\lambda m}^+ b_{\lambda m} + 1/2) \\
& + \sum_{m=0}^N [V_{mm+1} \sigma_m^+ \sigma_{m+1}^- + V_{m+1m} \sigma_{m+1}^+ \sigma_m^-]. \quad (12)
\end{aligned}$$

Note the introduction of local transition operators $\sigma_m^{\pm} \equiv (1/2)(\sigma_m^x \pm i\sigma_m^y)$ as well as creation ($b_{\lambda m}^+$) and annihilation ($b_{\lambda m}$) operators for the various vibrational modes. The electron–vibrational coupling at site m is denoted by $\kappa_{\lambda m} \equiv C_{\lambda m} \sqrt{2\hbar/M_{\lambda m} \omega_{\lambda m}}$. The quantities

$$E_0^{(\text{el})} = (1/2) \sum_m (E_m + \epsilon_m^{(0)}) \quad (13)$$

and

$$E_0^{(\text{nucl})} = \sum_m \sum_{\lambda} (\kappa_{\lambda m}^2 / 4\hbar \omega_{\lambda m}), \quad (14)$$

are independent on the concrete wire state and thus do not influence the ET process. The wire Hamiltonian, Eq. (12) has to be considered as the multi-site generalization of the ordinary spin-boson Hamiltonian.

Since our approach is aimed at a description of nonadiabatic charge motion based on a fast vibrational relaxation we will consider the vibrational modes as passive bath modes and perform a polaron transformation of the wire Hamiltonian H_W . Therefore, the unitary operator $\hat{S} = \prod_{m=0}^{N+1} \hat{S}_m$ is introduced containing the local unitary operators (see e.g. [44,54–57])

$$\hat{S}_m = \exp \left[(1/2) \hat{R}_m \sigma_m^z \right], \quad (15)$$

with

$$\hat{R}_m = \sum_{\lambda} g_{\lambda m} (b_{\lambda m}^+ - b_{\lambda m}), \quad (g_{\lambda m} \equiv \kappa_{\lambda m} / \hbar \omega_{\lambda m}). \quad (16)$$

If applied to the wire Hamiltonian we obtain

$$\tilde{H}_W = \hat{S} H_W \hat{S}^+ = E_0^{(\text{el})} + \tilde{H}_W^{(\text{el})} + \hat{V}_W^{(\text{tr})} + H_B. \quad (17)$$

The expression

$$\tilde{H}_W^{(\text{el})} = (1/2) \sum_{m=0}^{N+1} \epsilon_m \sigma_m^z, \quad (18)$$

is the electronic part of the transformed wire Hamiltonian

$$H_B = \sum_{m=0}^{N+1} \sum_{\lambda} \hbar \omega_{\lambda m} (b_{\lambda m}^+ b_{\lambda m} + 1/2), \quad (19)$$

defines the bath Hamiltonian (associated with the vibrational states of the wire and its surrounding), and

$$\hat{V}_W^{(\text{tr})} = \sum_{m=0}^N [V_{mm+1} \tilde{\sigma}_m^+ \tilde{\sigma}_{m+1}^- + V_{m+1m} \tilde{\sigma}_{m+1}^+ \tilde{\sigma}_m^-], \quad (20)$$

gives the modified off-diagonal interaction which is responsible for the ET processes in the wire. In the latter expression, we introduced

$$\tilde{\sigma}_m^{\pm} = \hat{S}_m \sigma_m^{\pm} \hat{S}_m^+ = \sigma_m^{\pm} e^{\pm \hat{R}_m}. \quad (21)$$

[We took into consideration the fact that $\sigma_m^+ \sigma_m^z - \sigma_m^z \sigma_m^+ = \pm 2\sigma_m^{\pm}$, and that $(\sigma_m^z)^n$ is equal σ_m^z (if n is the even integer) or 1 (if n is the odd integer).] The wire Hamiltonian, Eq. (17) is suitable for the description of long-range ET through the wire because the off-diagonal interaction (20) includes the coupling of a particular electronic state to the bath. (Beside this property one has to bear in mind that the pseudo-spin operators $\sigma_m^{x,y,z}$ commute if they refer to different sites m .)

Performing the polaron-transformation at the complete Hamiltonian of the LWR-system, $H_{\text{LWR}} = H_{\text{LWR}}^{(\text{el})} + H_W^{(\text{nucl})}$, we get

$$H = \tilde{H}_0 + V + H_B. \quad (22)$$

Here, H_B is given by Eq. (19), and we have

$$\tilde{H}_0 = H_{\text{LR}}^{(\text{el})} + \tilde{H}_W^{(\text{el})}, \quad (23)$$

and

$$V = \hat{V}_W^{(\text{tr})} + \hat{V}_{\text{LR-W}}^{(\text{tr})}. \quad (24)$$

In both equations the operators $H_{\text{LR}}^{(\text{el})}$, $\tilde{H}_W^{(\text{el})}$ and $\hat{V}_W^{(\text{tr})}$ are defined by the Eqs. (4), (18) and (20), respectively. Furthermore, we introduced

$$\begin{aligned}
\hat{V}_{\text{LR-W}}^{(\text{tr})} = & \sum_{\mathbf{k}} [V_{\text{Lk}} a_{\text{Lk}}^+ \tilde{\sigma}_0^- + V_{\text{Lk}}^* \tilde{\sigma}_0^+ a_{\text{Lk}}] \\
& + \sum_{\mathbf{q}} [V_{\text{Rq}} a_{\text{Rq}}^+ \tilde{\sigma}_{N+1}^- + V_{\text{Rq}}^* \tilde{\sigma}_{N+1}^+ a_{\text{Rq}}]. \quad (25)
\end{aligned}$$

The LWR-system Hamiltonian, Eq. (22) is the one on which all further derivations of kinetic equations will be based. Note that it does not contain the nuclear energy $E_0^{(\text{nucl})}$, Eq. (14) as it is the case for the nuclear Hamiltonian (12). The absence is originated by the polaron-transformation which leads to a complete compensation. The wire electronic energy $E_0^{(\text{el})}$, Eq. (13) has been omitted since it does not depend on the concrete electronic state.

3. Formation of an interelectrode current

Let us specialize the model of the LWR-system a little bit further. We provide for all what follows that the local LUMO-level energies ϵ_m of the various wire internal units ($m = 1, \dots, N$) are position considerably above the Fermi-levels E_F of the electrodes (cf. Fig. 1(a)). And for any applied voltage considered in the following these levels should not come into resonance with the Fermi-levels. Thus, direct long-ranged resonant tunneling is of no importance [58]. In contrast, the terminal wire units $m = 0$ and $m = N + 1$ should have a structure different from the internal wire part (originated, for example, by absorbed atoms, by atomic clusters at the wire–electrode interface, or by additional molecular groups which belong to the terminal units [20]). As a result the LUMO-

level energies ϵ_0 and ϵ_{N+1} may become degenerated with the electrode's Fermi-energies at a certain voltage. Therefore, only those transition processes as represented in scheme Fig. 1(a) are assumed to contribute to the formation of the interelectrode current I .

To derive an expression for the current I we start from the general relation

$$I = -e\dot{N}_L, \quad (26)$$

where e denotes the absolute value of the electron charge and $\dot{N}_L = -\dot{N}_R$ is the time-derivative of the number of those electrons moving through the molecular wire from the left (L) to the right (R) electrode. Since the total left electrode population reads as

$$N_L(t) = \sum_{\mathbf{k}} P_{L\mathbf{k}}(t), \quad (27)$$

we have to determine the time-derivative of the band-state population $P_{L\mathbf{k}}(t)$. This population is defined in the occupation number representation according to

$$\begin{aligned} P_{L\mathbf{k}}(t) &= \text{tr}(\rho(t)\hat{N}_{L\mathbf{k}}) \\ &= \sum_{N_{L\mathbf{k}}} \sum_{\{N_s\} \neq N_{L\mathbf{k}}} \langle N_{L\mathbf{k}}, \{N_s\} | \rho(t) | \{N_s\}, N_{L\mathbf{k}} \rangle N_{L\mathbf{k}}, \end{aligned} \quad (28)$$

with $\rho(t)$ denoting the electronic density matrix of the LWR-system. The electronic occupation number operator has the following form:

$$\hat{N}_{L\mathbf{k}} = \sum_{N_{L\mathbf{k}}=0,1} N_{L\mathbf{k}} |N_{L\mathbf{k}}\rangle \langle N_{L\mathbf{k}}|, \quad (29)$$

and is diagonal with respect to the occupation number states $|N_{L\mathbf{k}}\rangle$. In the same manner one can define the electronic populations $P_{R\mathbf{q}}(t)$ of the right electrode. The wire-site populations read

$$\begin{aligned} P_m(t) &= \text{tr}(\rho(t)\hat{N}_m) \\ &= \sum_{N_m} \sum_{\{N_s\} \neq N_m} \langle N_m, \{N_s\} | \rho(t) | \{N_s\}, N_m \rangle N_m, \end{aligned} \quad (30)$$

with

$$\hat{N}_m = \sum_{N_m=0,1} N_m |N_m\rangle \langle N_m|, \quad (31)$$

being the site occupation number operator. Note the general notation $P_j(t)$ with $j = L\mathbf{k}, R\mathbf{q}, 0, 1, \dots, N+1$ which covers all populations and which can be obtained from the occupation number distribution

$$P(N_j, t) = \sum_{\{N_s\} \neq N_j} \langle N_j, \{N_s\} | \rho(t) | \{N_s\}, N_j \rangle. \quad (32)$$

Here, the summation runs over a complete set of occupation numbers $\{N_s\}$ except N_j . Combining Eq. (32) with the Eqs. (30) and (31) one obtains

$$P_j(t) = \sum_{N_j=0,1} N_j P(N_j, t),$$

and

$$1 - P_j(t) = \sum_{N_j=0,1} N_j P(1 - N_j, t), \quad (33)$$

what yields

$$P_j(t) = P(1_j, t), \quad 1 - P_j(t) = P(0_j, t). \quad (34)$$

In particular, we may write ($m = 0, 1, \dots, N+1$)

$$\sigma_m^z(t) = \text{tr}(\rho(t)\sigma_m^z) = P(1_m, t) - P(0_m, t) = 2P_m(t) - 1. \quad (35)$$

Applying standard methods of nonequilibrium statistical mechanics [2,56,59–61] one may derive a closed set of kinetic equations for just all introduced populations (cf. Appendix A):

$$\begin{aligned} \dot{N}_L(t) &= -\chi_L + \Gamma_L P_0(t), \\ \dot{P}_0(t) &= -(\Gamma_L + \alpha_0 + k_1)P_0(t) + \chi_L + \beta_0 P_1(t) + k_2 P_{N+1}(t), \\ \dot{P}_1(t) &= -(\alpha + \beta_0)P_1(t) + \alpha_0 P_0(t) + \beta P_2(t), \\ \dot{P}_m(t) &= -(\alpha + \beta)P_m(t) + \alpha P_{m-1}(t) + \beta P_{m+1}(t), \\ \dot{P}_N(t) &= -(\alpha_N + \beta)P_N(t) + \alpha P_{N-1}(t) + \beta_N P_{N+1}(t), \\ \dot{P}_{N+1}(t) &= -(\Gamma_R + \beta_N + k_2)P_{N+1}(t) + \chi_R + \alpha_N P_N(t) + k_1 P_0(t), \\ \dot{N}_R(t) &= -\chi_R + \Gamma_R P_{N+1}(t). \end{aligned} \quad (36)$$

Here, the index m runs over the wire units $2, 3, \dots, N-1$, only. Forward hopping rates are denoted by $\alpha_0 \equiv k_{01}$, $\alpha_N \equiv k_{NN+1}$, $\alpha \equiv k_{mm+1}$ (for explanation see also Fig. 1(b)). The related backward rates are $\beta_0 \equiv k_{01}$, $\beta_N \equiv k_{N+1N}$, and $\beta \equiv k_{m+1m}$. Since the considered rates characterize single-electron transitions between neighboring wire units the corresponding kinetic equations as well as the rate constants (describing the hopping processes within the wire) can be derived in the Born approximation with respect to the inter-site couplings $V_{mm\pm 1}$ (cf. Hamiltonian (5)). Concrete expressions for each rate are given in Eq. (A.41). There, $(\text{FC})_{ms}$ denotes the Franck–Condon factor (cf. Eqs. (A.35) and (A.36)), and V_{ms} is the coupling between neighboring sites (m and $s = m \pm 1$). Based on the same Born approximation, one can specify the rate describing the ET between each electrode and the adjacent terminal unit of the wire. In the Eq. (36) these are the electrode–wire rates (χ_L, χ_R) and the wire–electrode rates (χ_{-L}, χ_{-R}). Concrete expressions for these rates can be found in Eq. (A.45). The quantities

$$\Gamma_{L(R)} \equiv \chi_{L(R)} + \chi_{-L(-R)}, \quad (37)$$

determine the broadening of the 0th ($(N+1)$ th) terminal electronic wire level. The broadening is caused by the interaction of these levels with the conduction band levels of the left (right) electrode as well as by the coupling to vibrational modes. If the latter coupling van-

ishes $\Gamma_{L(R)}$ reduces to the standard expression for electronic level broadening [28,30,37].

Along with a standard sequential site-to-site ET process the set (36) contain contributions which result from the distant superexchange coupling V_{0N+1} , Eq. (A.51) between the terminal units of the wire 0 and $N+1$. There are two superexchange ET rates, the wire internal forward rate $k_1 \equiv k_{0N+1}$ and the backward rate $k_2 \equiv k_{N+10}$, defined by Eq. (A.50). Details of the derivation of the basic set of coupled linear kinetic equations (36) are given in Appendix A. [Note that a linear form of set of equations is only valid for bulk electrodes where the Eq. (A.44) is fulfilled in LWR system. Besides, the population of each interior wire unit has to be small during the ET process, cf. Eq. (A.39).]

Having established the set (36) of kinetic equations we will restrict ourselves to the consideration of its stationary solution only. It allows to characterize the stationary ET regime where $\dot{P}_m = 0$, and $\dot{N}_L = -\dot{N}_R = \text{const}$. Noting the first relation the set of equations for the site populations P_m can be solved exactly. Then, the substitution of the solution for P_0 into the first equation of the set (36) leads to the following analytic expression for the interelectrode current:

$$I = e \frac{\chi_L \Gamma_R A_{N+1} - \chi_R \Gamma_L A_0}{\Gamma_L A_0 + \Gamma_R A_{N+1}}. \quad (38)$$

The newly introduced constants A_0 and A_{N+1} read as

$$\begin{aligned} A_0 = & (\chi_L + \chi_R) \{ k_2 [(\alpha\alpha_N + \beta\beta_0 + \alpha_N\beta_0)D(N-2) \\ & - (\alpha_N + \beta_0)\alpha\beta D(N-3)] + \beta_0\beta_N\beta^{N-1} \} \\ & + \chi_L \Gamma_R [(\alpha\alpha_N + \beta\beta_0 + \alpha_N\beta_0)D(N-2) \\ & - (\alpha_N + \beta_0)\alpha\beta D(N-3)], \end{aligned} \quad (39)$$

and

$$\begin{aligned} A_{N+1} = & (\chi_L + \chi_R) \{ k_1 [(\alpha\alpha_N + \beta\beta_0 + \alpha_N\beta_0)D(N-2) \\ & - (\alpha_N + \beta_0)\alpha\beta D(N-3)] + \alpha_0\alpha_N\alpha^{N-1} \} \\ & + \chi_R \Gamma_L [(\alpha\alpha_N + \beta\beta_0 + \alpha_N\beta_0)D(N-2) \\ & - (\alpha_N + \beta_0)\alpha\beta D(N-3)]. \end{aligned} \quad (40)$$

Both foregoing formulas contain the quantity

$$D(M) = (\alpha\beta)^{M/2} \frac{\sinh[A(M+1)]}{\sinh A}, \quad (e^{-A} = (\beta/\alpha)^{1/2}), \quad (41)$$

which mainly determines the length-dependence of the hopping contribution to the total interelectrode current.

4. Analytic expression for the current

The Eqs. (38)–(40) enable us to compute the I – V characteristics of the wire for different ratios among the rate constants. To get a somewhat simpler expression

ready to study the wire-length dependence of the current we will specify the geometry of the wire (sites of electron localization) as well as the relations among the forward and the backward transfer rates. In the case of non-adiabatic ET under consideration the intersite electronic couplings $V_1 \equiv V_{10}$, $V_B \equiv V_{mm+1}$ ($m = 1, 2, \dots, N$), and $V_N \equiv V_{NN+1}$ (see Fig. 1(a)) are assumed to be small. Therefore, it is not necessary to introduce extended LUMO wire level. Just the local site energies E_m determine the direction of the ET process. To derive a concrete expression for the energies E_m we suppose that the transferred electron captured by a wire unit is located at the center of this unit. Furthermore, we introduce l_0 and l_{N+1} as the distances between the centers of the left and the right terminal wire unit and the corresponding left and right electrode, respectively. l_1 and l_N denote the distances between the centers of the terminal units and the adjacent right (1th) and left (N th) wire units. Finally, l is the distance between the remaining internal wire centers. Then we get the voltage dependent site energies as

$$E_0 = E_0^{(0)} - eV(l_0/d), \quad (42)$$

$$E_{N+1} = E_{N+1}^{(0)} - eV[1 - (l_{N+1}/d)], \quad (43)$$

$$\begin{aligned} E_m = & E_m^{(0)} - eV(1/d)[l_0 + l_1 + (m-1)l], \\ & (m = 1, 2, \dots, N). \end{aligned} \quad (44)$$

Here, the distance between the two electrodes is given by

$$d = l_0 + l_1 + (N-1)l + l_N + l_{N+1}. \quad (45)$$

According to the given expressions for the site energies we remind on the detailed balance relations among the different rate expressions, which read

$$\begin{aligned} \alpha_0 = & \beta_0 \exp(-\Delta E_1/k_B T), \\ \beta_N = & \alpha_N \exp(-\Delta E_N/k_B T), \\ \beta = & \alpha \exp(-\Delta E_m/k_B T), \quad (m = 1, \dots, N-1), \end{aligned} \quad (46)$$

and

$$k_2 = k_1 \exp(-\Delta E/k_B T). \quad (47)$$

The corresponding energy gaps are defined as

$$\begin{aligned} \Delta E_1 = & (E_1 + \varepsilon_0^{(0)}) - (E_0 + \varepsilon_1^{(0)}) = \Delta\varepsilon_1 - eV(l_1/d), \\ (\Delta\varepsilon_1 = & (E_1^{(0)} + \varepsilon_0^{(0)}) - (E_0^{(0)} + \varepsilon_1^{(0)})), \end{aligned} \quad (48)$$

$$\Delta E_N = (E_N + \varepsilon_{N+1}^{(0)}) - (E_{N+1} + \varepsilon_N^{(0)}) = \Delta\varepsilon_N + eV(l_N/d),$$

$$(\Delta\varepsilon_N = (E_N^{(0)} + \varepsilon_{N+1}^{(0)}) - (E_{N+1}^{(0)} + \varepsilon_N^{(0)})), \quad (49)$$

$$\Delta E_m = (E_m + \varepsilon_{m+1}^{(0)}) - (E_{m+1} + \varepsilon_m^{(0)}) = eV(l/d), \quad (50)$$

and

$$\begin{aligned}\Delta E &= \left(E_0 + \varepsilon_{N+1}^{(0)}\right) - \left(E_{N+1} + \varepsilon_0^{(0)}\right) \\ &= \Delta\varepsilon + eV[1 - (l_0 + l_{N+1})/d], \\ (\Delta\varepsilon &= \left(E_0^{(0)} + \varepsilon_{N+1}^{(0)}\right) - \left(E_{N+1}^{(0)} + \varepsilon_0^{(0)}\right)).\end{aligned}\quad (51)$$

For the sake of definiteness we assumed zero voltage at the left electrode (remember $e > 0$).

Analogous relation among the rate constants of the transitions between the electrodes and adjacent terminal wire units read as

$$\chi_{L(R)} = \chi_{-L(-R)} \exp(-\Delta E_{L(R)}/k_B T). \quad (52)$$

The site-electrode energy gaps are

$$\begin{aligned}\Delta E_L &= E_0 - \left(\varepsilon_0^{(0)} + E_F\right) = \Delta\varepsilon_L - eV(l_0/d), \\ (\Delta\varepsilon_L &= E_0^{(0)} - \left(\varepsilon_0^{(0)} + E_F\right)),\end{aligned}\quad (53)$$

and

$$\begin{aligned}\Delta E_R &= E_{N+1} - \varepsilon_0^{(N+1)} - (E_F - eV) = \Delta\varepsilon_R + eV(l_{N+1}/d), \\ (\Delta\varepsilon_R &= E_0^{(N+1)} - \left(\varepsilon_0^{(N+1)} + E_F\right)).\end{aligned}\quad (54)$$

Below we will consider the formation of an electronic current from the left to the right electrode, i.e., at $V > 0$. It follows from relations (46)–(54) that

$$\begin{aligned}\chi_{-L}\chi_R\beta_0\beta_N\beta^{N-1} &= \chi_{-R}\chi_L\alpha_0\alpha_N \exp(-eV/k_B T), \\ \chi_R\chi_{-L}k_2 &= \chi_{-R}\chi_Lk_1 \exp(-eV/k_B T).\end{aligned}\quad (55)$$

Therefore, expression (38) can reduce to the more compact form

$$I = e[1 - \exp(-eV/k_B T)] \frac{\chi_L}{\Gamma_L} \frac{F_1}{F_2}, \quad (56)$$

where

$$F_1 = k_1 \left(\frac{1 - \gamma^{N-1}}{1 - \gamma} + \frac{\alpha}{\beta_0} + \frac{\alpha}{\alpha_N} \gamma^{N-1} \right) + \frac{\alpha_0}{\beta_0} \alpha, \quad (57)$$

$$\begin{aligned}F_2 &= \left(1 + \frac{k_1}{\Gamma_L} + \frac{k_2}{\Gamma_R} \right) \left(\frac{1 - \gamma^{N-1}}{1 - \gamma} + \frac{\alpha}{\beta_0} + \frac{\alpha}{\alpha_N} \gamma^{N-1} \right) \\ &\quad + \frac{\alpha\alpha_0}{\Gamma_L\beta_0} + \frac{\alpha\beta_N}{\Gamma_R\alpha_N} \gamma^{N-1}.\end{aligned}\quad (58)$$

The parameter

$$\gamma \equiv \beta/\alpha = \exp(-eV/dk_B T), \quad (59)$$

characterizes the ratio between the backward and the forward wire-internal inter-site ET rate constants.

Eqs. (56)–(58) define the final analytic expression for the current. This expression has been obtained from the *exact* stationary solution of the set of rate equations (36) and shows a mixture of the two superexchange rate constants k_1 and k_2 and the remaining sequential rate

constants. Such a mixture results in a rather complicated dependence of the current on the number N of wire units. If, however, the inequalities

$$k_1, \alpha_0 \ll \Gamma_L, \quad k_2, \beta_N \ll \Gamma_R, \quad (60)$$

are fulfilled the current (56) reduces to the sum of two separate contributions

$$I = [1 - \exp(-eV/k_B T)] [I_{\text{sup}}(N) + I_{\text{seq}}(N)]. \quad (61)$$

The superexchange component of the interelectrode current reads

$$I_{\text{sup}}(N) = e(\chi_L/\Gamma_L)k_1. \quad (62)$$

This expression indicates that the distant dependence of the superexchange contribution is concentrated in the rate constant k_1 defined in Eq. (A.50). Below we consider the distant behavior of the current at such voltages which do not essentially alternate the gaps (A.49). In this case the simplified form of the superexchange coupling, Eq. (A.53) is valid. It allows to reduce Eq. (62) to the expression

$$I_{\text{sup}}(N) = I_{\text{sup}}^{(0)} e^{-\zeta(N-1)}, \quad (63)$$

where

$$\zeta = -2 \ln \left[|V_B| / \sqrt{\Delta E_0 \Delta E_{N+1}} \right], \quad (64)$$

and

$$I_{\text{sup}}^{(0)} = e(\chi_L/\Gamma_L)k_1^{(0)}, \quad (65)$$

$$k_1^{(0)} = \frac{2\pi}{\hbar} \frac{|V_1 V_{N+1}|^2}{\Delta E_0 \Delta E_{N+1}} (\text{FC})_{0N+1}. \quad (66)$$

As to the sequential component it has the form

$$I_{\text{seq}}(N) = I_{\text{seq}}^{(0)} \left[1 + \xi \frac{1 - \gamma^{N-1}}{1 - \gamma} \right]^{-1}, \quad (67)$$

with

$$I_{\text{seq}}^{(0)} = e \frac{\chi_L}{\Gamma_L} \frac{\alpha_0 \alpha_N}{\beta_0 + \alpha_N}, \quad (68)$$

and

$$\xi = \frac{1 - (\alpha/\alpha_N)(1 - \gamma)}{(\alpha/\beta_0) + (\alpha/\alpha_N)}. \quad (69)$$

The analytic dependence of each component on the bridge unit number N is provided by the diminishing parameters (64) and (69). Note that the diminishing parameter ξ valid for the sequential transfer is defined through elementary rate constants. Thus, the suppression of the sequential part of the current is defined by kinetic processes. In contrast, the superexchange diminishing parameter ζ reflects the dynamic properties of the wire.

5. Discussion of the results

The exact expression, Eq. (56) for the wire mediated current as well as the approximated ones, Eqs. (63) and (67) have to be considered as the main results of the present work. In particular, these formulas allow us to analyze the dependence of the current on the number of wire units, and in this way, to specify the concrete mechanism of the interelectrode current formation through the molecular wire. To present some numerical results we will use Jortner's expression for the various site-site rate constants (see Appendix A, Eqs. (A.41), (A.37) and (A.38)). They are given by

$$\beta_0 = \frac{2\pi}{\hbar} \frac{|V_1|^2}{\hbar\omega_1} \Phi_{v_1}, \quad (70)$$

$$\alpha_N = \frac{2\pi}{\hbar} \frac{|V_N|^2}{\hbar\omega_N} \Phi_{v_N}, \quad (71)$$

$$\alpha = \frac{2\pi}{\hbar} \frac{|V_B|^2}{\hbar\omega_B} \Phi_{v_B}, \quad (72)$$

$$k_1 = \frac{2\pi}{\hbar} \frac{|V_{0N+1}|^2}{\hbar\Omega} \Phi_v, \quad (73)$$

where ω_1 , ω_N , ω_B and Ω are the characteristic vibrational frequencies related to $1 \rightarrow 0$, $N \rightarrow N+1$, $m \rightarrow m+1$ and $0 \rightarrow N+1$ electron transitions, respectively. The corresponding reorganization energies are denoted by $E_1^{(r)}$, $E_N^{(r)}$, $E_B^{(r)}$ and $E^{(r)}$. In Eqs. (70)–(73), each function Φ_{v_i} (cf. definition (A.38)) depends on two parameters: $S_1 = E_1^{(r)}/\omega_1$ and $v_1 = \Delta E_1/\omega_1$ (function Φ_{v_1}), $S_N = E_N^{(r)}/\omega_N$ and $v_N = \Delta E_N/\omega_N$ (function Φ_{v_N}), $S_B = E_B^{(r)}/\omega_B$ and $v_B = \Delta E_m/\omega_B$ (function Φ_{v_B}), and $S = E^{(r)}/\Omega$ and $v = \Delta E/\Omega$ (function Φ_v). [Note that the gaps ΔE_1 , ΔE_N , ΔE_m and ΔE are defined through relations (48)–(51).]

The electrode-wire transfer rates have been chosen in the form [41,42]

$$\chi_{-L(-R)} = \chi_0 [1 - n_F(\Delta E_{L(R)})] \Phi_0^{(L(R))}, \quad (74)$$

where $n_F(\Delta E_{L(R)}) = [\exp(\Delta E_{L(R)}/k_B T) + 1]^{-1}$ is the Fermi distribution function with the energy gaps defined in the Eq. (53) as well as (54), and we introduced

$$\Phi_0^{(L)} = e^{-S_0 \coth(\hbar\omega_0/k_B T)} I_0 \left(2S_0 [n(\omega_0)(1 + n(\omega_0))]^{1/2} \right). \quad (75)$$

[The quantity $\Phi_0^{(R)}$ follows from $\Phi_0^{(L)}$ by replacing $S_0 = E_0^{(r)}/\omega_0$ and ω_0 by $S_{N+1} = E_{N+1}^{(r)}/\omega_{N+1}$ and ω_{N+1} , respectively.] In Eq. (74), χ_0 is the width of a single electronic level caused by the interaction with one of the two electrodes in the absence of electron-vibration coupling. This conclusion is based on the definition of the level broadenings $\Gamma_{L(R)}$, Eq. (37). Actually, for a

symmetric wire and in the absence of electron-vibration coupling where $\Phi_0^{(L(R))}$ equals one, it follows $\Gamma_L = \Gamma_R = \chi_0$.

Fig. 2 demonstrates the agreement between the exact and the approximate description of the current, thus supporting the conclusion that the additive form of the current, Eq. (61) is sufficiently correct if the inequalities (60) are fulfilled. If this is not the case, there is a difference in the wire-length dependence of the current, Fig. 3. This difference is more significant for a small number of wire units at which the influence of the superexchange ET channel is larger. Fig. 4 shows that the superexchange channel becomes dominant if the current is measured at lower temperature. Note, however, that the drop of the superexchange component does not follow the conventional dependence $I_{\text{sup}} \sim \exp[-\zeta(N-1)]$ (see the curve at $T = 180$ K). This is due to the fact that Eq. (63) contains an additional weak dependence on N via $I_{\text{sup}}^{(0)}$, Eq. (65). Indeed, $I_{\text{sup}}^{(0)}$ is proportional to the rate $k_1^{(0)}$, Eq. (66) which in turn is proportional to the Franck-Condon factor (FC) $_{0N+1}$. This Franck-Condon factor depends on the driving force $\Delta E = \epsilon_0 - \epsilon_{N+1} = \Delta\epsilon^{(0)} - eV[l_1 + l_N + l(N-1)]$, Eq. (51) which for $V \neq 0$ is a function of the number of wire units connecting the sites 0 and $N+1$. Therefore, we may conclude that the superexchange part of the current results in a slightly corrected exponential decrease with increasing N , while the sequential part shows a smooth decrease.

The N -dependence of I_{seq} is contained in the factor $(1 - \gamma^{N-1})/(1 - \gamma)$ which has the two limits, $N-1$ (at

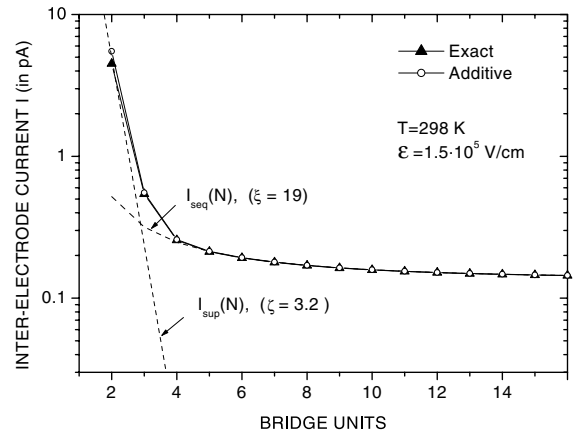


Fig. 2. Length-dependence of the interelectrode current at a fixed strength of the applied electric field $\mathcal{E} = V/d = 1.5 \times 10^5$ V/cm. The description based on the exact expression, Eq. (56), and the approximate one, Eq. (61) coincide. As a consequence, the current can be represented in this case as an additive contribution of the superexchange ET mechanisms and the sequential mechanism. The rate constants are defined by Eqs. (70)–(74) with the parameters $\Delta\epsilon_0 = \Delta\epsilon_{N+1} = 0.1$ eV, $\Delta\epsilon_1 = \Delta\epsilon_N = 0.25$ eV, $\Delta\epsilon = 0$, $E_0^{(r)} = E_{N+1}^{(r)} = 0.7$ eV, $E_1^{(r)} = E_N^{(r)} = 0.4$ eV, $E_B^{(r)} = 0.6$ eV, $E^{(r)} = 0.2$ eV, $V_1 = V_N = 0.02$ eV, $V_B = 0.03$ eV, $\omega_0 = \omega_{N+1} = 800$ cm^{-1} , $\omega_1 = \omega_N = \omega_B = \Omega = 50$ cm^{-1} , $\chi_0 = 10^{13}$ s^{-1} , $l_0 = l_{N+1} = 4$ \AA , $l_1 = l_N = l = 3$ \AA .

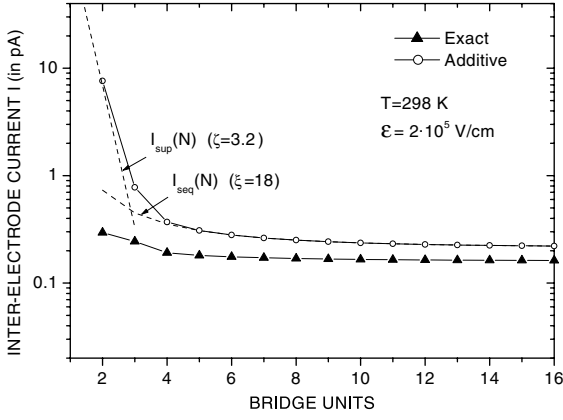


Fig. 3. Length-dependence of the interelectrode current at a fixed strength of the applied electric field $\mathcal{E} = V/d = 2 \times 10^5$ V/cm. There occurs a distinct difference between the exact expression, Eq. (56) and the approximate theory, see Eq. (61). The set of parameters are the same as in Fig. 2 except $\omega_0 = \omega_{N+1} = 50$ cm $^{-1}$, $\omega_1 = \omega_N = \omega_B = \Omega = 100$ cm $^{-1}$.

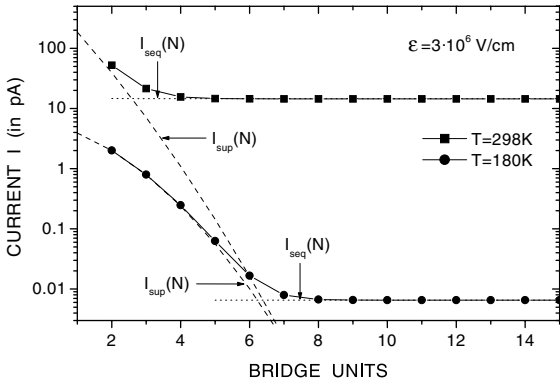


Fig. 4. Length-dependence of the interelectrode current at a fixed strength of the applied electric field $\mathcal{E} = V/d = 3 \times 10^6$ V/cm and for two different temperatures at $T = 298$ K and at $T = 180$ K. The description is based on the exact result (56). The approximate description using Eq. (61), is depicted by dashed lines. The deviation from an exponential decrease of the superexchange component of the current can be clearly identified. The rate constants are defined according to the Eqs. (70)–(74) with parameters $\Delta\varepsilon_0 = \Delta\varepsilon_{N+1} = 0.1$ eV, $\Delta\varepsilon_1 = \Delta\varepsilon_N = 0.4$ eV, $\Delta\varepsilon = 0$, $E_0^{(r)} = E_{N+1}^{(r)} = 0.7$ eV, $E_1^{(r)} = E_N^{(r)} = 0.8$ eV, $E_B^{(r)} = 0.6$ eV, $E^{(r)} = 1$ eV, $V_1 = V_N = 0.05$ eV, $V_B = 0.07$ eV, $\omega_0 = \omega_{N+1} = 800$ cm $^{-1}$, $\omega_1 = \omega_N = \omega_B = \Omega = 50$ cm $^{-1}$, $\chi_0 = 10^{13}$ s $^{-1}$, $l_0 = l_{N+1} = 4$ Å, $l_1 = l_N = l = 3$ Å.

$\gamma \approx 1$), and 1 (at $\gamma \ll 1$). Therefore, the sequential contribution to the total current shows to limiting cases

$$I_{\text{seq}}(N) = \frac{I_{\text{seq}}^{(0)}}{1 + \zeta(N-1)},$$

$$\zeta = \frac{1}{(\alpha/\beta_0) + (\alpha/\alpha_N)}, \quad (\beta \approx \alpha), \quad (76)$$

and

$$I_{\text{seq}}(N) = \frac{I_{\text{seq}}^{(0)}}{1 + \zeta},$$

$$\zeta = \frac{1 - (\alpha/\alpha_N)}{(\alpha/\beta_0) + (\alpha/\alpha_N)}, \quad (\beta \ll \alpha). \quad (77)$$

In the first limit, Eq. (76), $I_{\text{seq}}(N)$ shows a hyperbolic decrease with increasing N . Such a behavior of the current is caused by the presence of hopping processes for which the forward and backward wire-internal intersite rate constants are equal one to another. Physically, this case corresponds to a small intersite voltage bias so that $\exp(-eVl/dk_B T) \approx 1$. The second limit, Eq. (77), is realized for a large intersite voltage bias when $\exp(-eVl/dk_B T) \ll 1$. Here, the ET along the regular part of the wire is exclusively defined by the forward rate constant α . It corresponds to a directed ET in the wire so that the interelectrode current does not depend on the number of wire units. Both limiting cases clearly indicate that at a large number of wire units the sequential mechanism prevails the superexchange one. Such a conclusion follows from the additive form of the current, Eq. (61) and additionally, if the conditions for deep tunneling are fulfilled. As a matter of fact, the additive form of the current is obtained if, and only if, the inequalities (60) are fulfilled in the course of the ET. Furthermore, in this case all site populations P_m related to the internal wire units $m = 1, 2, \dots, N$ become small.

Note that above mentioned N -dependence of the sequential contribution to the total current is only valid if this dependence is studied at a fixed strength of the applied electric field $\mathcal{E} = V/d$. Just in this case the ratio (59) becomes a length-independent parameter. Thus the length dependence of the hopping component of the current is only given by the factor γ^{N-1} (see Eqs. (56)–(58) as well as Eqs. (61) and (67)). Such a result does not remain valid if the N -dependence is studied for a fixed voltage V (see also the discussion in [62]). Fig. 5

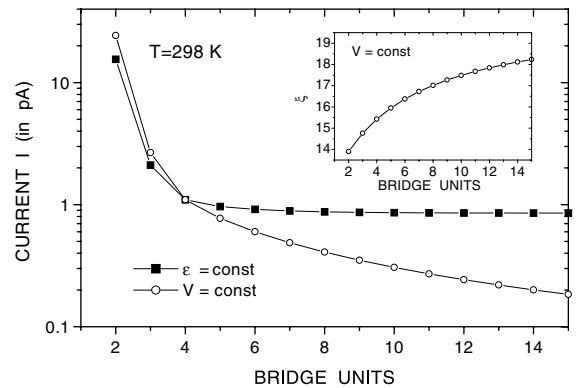


Fig. 5. Length-dependence of the interelectrode current at a fixed strength of the applied electric field $\mathcal{E} = V/d = 4.35 \times 10^5$ V/cm and at a voltage $V = 0.9$ V. There occurs a strong difference in the wire-length dependence which is caused by the contribution corresponding the sequential ET. The insert depicts the variation of the sequential diminishing parameter ζ as a function of the wire length. The description is based on the exact Eq. (56). The parameters are the same as those for Fig. 2.

illustrates this statement. If the N -dependence is studied at $V = \text{const.}$, the sequential diminishing parameter ζ exhibits an additional N -dependence (see inset in Fig. 5). It follows from the ratio (59) of the backward and the forward intersite rate constants and by the electrode–electrode distance d , Eq. (45).

6. Conclusions

In the present paper, we have generalized the spin-boson model to a description of nonadiabatic electron transfer (ET) processes which take place in systems with an arbitrary number of localization sites of the excess electron. Site pseudo-spin operators (9)–(11) have been introduced and a Hamiltonian (22) has been presented which describes the ET in the system “left (L) electrode–molecular wire–right (R) electrode”. The linear coupling of the excess electron levels to nuclear vibrations was taken into account in an exact manner by carrying out the well-known polaron transformation (15). After such a transformation the coupling among the electronic levels is combined with a coupling to the nuclear vibrations, Eq. (24), and in turn becomes a weak perturbation. The used local pseudo-spin operators act in the space of occupation number states. Correspondingly, we have derived a master equation for the occupation number distribution, Eq. (A.28). This equation presents a key-result for the unified description of charge motion through a molecular wire. We arrived at a set of kinetic equations for state populations including corresponding sequential and superexchange ET rate constants. It is of prominent importance to utilize the occupation number representation, since it easily allows to consider Pauli’s exclusion principle which results in a nonlinearity in the kinetic equations (A.34) and (A.42).

The generalization of the spin-boson model to the description of charge motion through molecular wires has been done for the case of thermally activated interelectrode transfer. In this case, the transferred electron is released from the electrode to the adjacent terminal unit of the wire. Afterwards the electron either moves through the wire units (the sequential pathway) or it performs a single transition to the terminal group at the other tail of the wire (the superexchange pathway). A particular model has been considered for which the wire-internal units $1, 2, \dots, N$ (cf. the scheme in Fig. 1) act as a bridging molecular structure between the terminal units. This model also ensures that these units are only weakly populated by the transferred electron. Resulting from this we may utilize a linear version of the kinetic equations, Eq. (36). In this connection it is important that we have been able to derive the exact solution of these kinetic equations and thus to have at hand an analytic form for the interelectrode current

(Eqs. (38)–(41)). Taking the exact (Eqs. (56)–(58)) as well as approximated analytic expressions for the current (Eqs. (61)–(67)) we have analyzed its length-dependence at a fixed electric field $\mathcal{E} = V/d$ as well as at a fixed voltage V . Such an analysis of the wire-length dependence of the current allowed us to draw the following conclusions.

(1) The general case of interelectrode current formation there is a strong mixing between the sequential and the superexchange mechanism, note the exact expression for the current, Eq. (56). An naive, additive contribution of both mechanisms, see Eq. (61) only becomes justified if the specific conditions, Eq. (60) are fulfilled. Physically, these conditions correspond to a fast ET between the electrodes and the adjacent wire units. (Then, an ET is defined by the integral level broadenings Γ_L and Γ_R , Eq. (37).)

(2) If $V > V_{\text{res}}$, where V_{res} is defined by the gap between the terminal LUMO-level energy ϵ_0 , Eq. (1) and the Fermi-level E_F , a resonant ET from electrode L to the terminal wire unit 0 occurs. Furthermore, the site–electrode transition rate χ_{-L} becomes small compared to the electrode–site rate χ_L , so that Γ_L starts to coincide with χ_L . This means that a release of an electron from electrode L to the terminal wire unit 0 does not require thermal activation. Therefore, the part of the current based on the superexchange ET between the terminal wire units is also present at low temperatures. This fact is illustrated by Eqs. (65) and (66), and Fig. 4.

(3) There exists a distinct difference in the wire-length dependence of the current found at a fixed electric field $\mathcal{E} = V/d$ and at a fixed voltage V (cf. Fig. 5). This difference is caused by several factors. First of all, if $\mathcal{E} = V/d = \text{const.}$ the parameter γ , Eq. (59) as well as the rate constants α , β , $\alpha_{0(N)}$ and $\beta_{0(N)}$ (defining the sequential ET channel) become wire-length independent quantities. Therefore, the N -dependence of the sequential component of the current is completely defined by the factor γ^{N-1} (or/and $(1 - \gamma^{N-1})/(1 - \gamma)$). In contrast, the superexchange site–site coupling defined by Eq. (A.51) includes an N -dependence only via the number of inter-wire transfer couplings, thus it can be approximated by the simplified expression (A.53). The latter contains the diminishing parameter ζ , Eq. (64), which does not depend on N . Therefore, at $\mathcal{E} = V/d = \text{const.}$ the superexchange component of the current shows a weak deviation from an exponential law $\sim \exp[-\zeta(N - 1)]$ caused by the dependence of the driving force ΔE , Eq. (51) on N . The length-dependence of the current becomes more complicated if the current is measured at $V = \text{const.}$ In this case all rate constants depend on N due to the dependence of the driving forces, which all belong to separate ET reactions, Eqs. (48)–(51) on the distance d . Additionally, the ratio (59) and the superexchange coupling (A.51) also show the N -dependence. Thus, the length-dependence of the current is much

more complex as compared to the case of bridge-mediated donor–acceptor ET [52].

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Appendix A. Master equation in the occupation number representation and kinetic equations

In the case of the considered nonadiabatic ET the transition processes take place on a time scale Δt which significantly exceeds the characteristic time τ_{rel} of vibrational relaxation. Following from this the vibrational degrees of freedom can be considered as a thermal bath. Moreover, the considered regime of ET can be characterized by a certain property of the total density operator $\rho^{(S-B)}(t)$ of the LWR-system (including the vibrational degrees of freedom). This property is related to the part $\rho_d^{(S-B)}(t)$ of $\rho^{(S-B)}(t)$ which is diagonal in a representation based on the used local electronic states and the related vibrational states. We have

$$\lim_{t \gg \tau_{\text{rel}}} \rho_d^{(S-B)}(t) = W_B \rho_d(t), \quad (\text{A.1})$$

where $\rho_d(t)$ is the diagonal part of the electronic density operator (taken in the mentioned basis). The latter is defined according to the standard expression

$$\rho(t) = \text{tr}_{\text{vib}} \rho^{(S-B)}(t), \quad (\text{A.2})$$

where tr_{vib} denotes the trace with respect to all vibrational states. Finally, we also introduced

$$W_B = \exp(-H_B/k_B T) / \text{tr}_{\text{vib}} \exp(-H_B/k_B T), \quad (\text{A.3})$$

which is the equilibrium vibrational (bath) density operator. The factorization ansatz (A.1) corresponds to a basic assumption of nonequilibrium statistical mechanics (see, e.g. [2,56,59,61]). If \hat{O} is an electronic operator which is diagonal in the mentioned basis then the corresponding average can be derived according to

$$\bar{O}(t) = \text{tr}(\rho(t)\hat{O}) = \text{tr}(\rho_d(t)\hat{O}). \quad (\text{A.4})$$

Consequently, only the diagonal part of the electronic density operator $\rho_d(t)$ is important for the determination of $\bar{O}(t)$. Indeed, this is the case when evaluating the electronic state populations $P_{\text{Lk}}(t)$ and $P_{\text{Rq}}(t)$ for the electrodes as well as the site populations $P(N_m, t)$ for the wire units $m = 0, 1, \dots, N+1$ (see definition (32)).

Our next aim will be the derivation of kinetic equations for the population number distributions $P(N_j, t)$ ($j = \text{Lk}, \text{Rq}, 0, 1, \dots, N+1$). In doing this we note that the occupation number operators \hat{N}_j replace the diagonal operator \hat{O} introduced so far. The eigenstates of the LWR system are defined by the set of occupation numbers $\{N_j = 0, 1\}$ and read

$$|a\rangle \equiv |\{N_j\}\rangle = \prod_{\mathbf{k}} |N_{\text{Lk}}\rangle \prod_{\mathbf{q}} |N_{\text{Rq}}\rangle \prod_{m=0}^{N+1} |N_m\rangle. \quad (\text{A.5})$$

Therefore, we get

$$\begin{aligned} P(N_{\text{Lk}}, t) &= \sum_{a \neq N_{\text{Lk}}} \rho_{aa}(t) \\ &= \sum_{\{N_s\} \neq N_{\text{Lk}}} \langle N_{\text{Lk}}, \{N_s\} | \rho(t) | \{N_s\}, N_{\text{Lk}} \rangle, \end{aligned} \quad (\text{A.6})$$

where the summation covers all occupation numbers $\{N_j\}$ except N_{Lk} . In an analogous way we obtain for the distribution function of the wire-site populations

$$\begin{aligned} P(N_m, t) &= \sum_{a \neq N_m} \rho_{aa}(t) \\ &= \sum_{\{N_s\} \neq N_m} \langle N_m, \{N_s\} | \rho(t) | \{N_s\}, N_m \rangle. \end{aligned} \quad (\text{A.7})$$

Denoting the diagonal elements of the electronic density matrix (in the occupation number representation) as

$$\mathcal{P}_a(t) \equiv \rho_{aa}(t) = \langle a | \rho(t) | a \rangle = \langle a | \rho_d(t) | a \rangle, \quad (\text{A.8})$$

then it becomes obvious that

$$P(N_j, t) = \sum_{a \neq N_j} \mathcal{P}_a(t), \quad (j = \text{Lk}, \text{Rq}, 0, 1, \dots, N+1). \quad (\text{A.9})$$

Therefore, the derivation of kinetic equations for the populations $P(N_j, t)$ may be based on the master equation for $\mathcal{P}_a(t)$ or, what is equivalent, on the master equation for the diagonal density operator $\rho_d(t)$.

A.1. Master equation for the diagonal components of the density matrix of an open quantum system

Following the approach which leads to the well-known Nakajima–Zwanzig equation (see details in [61]) we introduce the projection operators \hat{T}_d and $\hat{T}_{nd} = 1 - \hat{T}_d$. They separate any operator $A = \sum_{ab} A_{ab} |a\rangle\langle b|$ expanded with respect to the basis states defined in Eq. (A.5) into diagonal and off-diagonal components:

$$\begin{aligned} \hat{T}_d A &= A_d = \sum_a A_{aa} |a\rangle\langle a|, \\ \hat{T}_{nd} A &= A_{nd} = \sum_{ab} (1 - \delta_{ab}) A_{ab} |a\rangle\langle b|. \end{aligned} \quad (\text{A.10})$$

Of course, the definition of the projection operators becomes unambiguously only since we related the definition to a particular basis set.

In the following we will identify the arbitrary operator A with $\rho^{(S-B)}(t)$ which is governed by the Liouville-von Neumann equation

$$\dot{\rho}^{(S-B)}(t) = -i\mathcal{L}\rho^{(S-B)}(t), \quad (\text{A.11})$$

$\mathcal{L} \equiv (1/\hbar)[H, \dots]$ is the Liouville superoperator specified by the total Hamiltonian $H = H_0 + V$. According to this separation we may write $\mathcal{L} = \mathcal{L}_0 + \mathcal{L}_V$ with $\mathcal{L}_0 \equiv (1/\hbar)[H_0, \dots]$, $\mathcal{L}_V \equiv (1/\hbar)[V, \dots]$. In the studied case of the LWR-system the Hamiltonian H is given by Eq. (22) and thus we may identify

$$H_0 = \tilde{H}_0 + H_B, \quad (\text{A.12})$$

with \tilde{H}_0 and H_B given in the Eqs. (23) and (19), respectively. Moreover, the interaction V is defined by Eq. (24) together with the Eqs. (20) and (25).

Utilizing the initial condition in the standard form $\rho_{nd}^{(S-B)}(0) = 0$ (decoupling of the system from the bath) and bearing in mind the properties

$$\hat{T}_d \mathcal{L}_0 \rho^{(S-B)}(t) = 0, \quad (\text{A.13})$$

$$\hat{T}_{nd} \mathcal{L}_0 \rho_d^{(S-B)}(t) = 0, \quad (\text{A.14})$$

$$\hat{T}_{nd} \mathcal{L}_0 \rho^{(S-B)}(t) = \mathcal{L}_0 \rho_{nd}^{(S-B)}(t), \quad (\text{A.15})$$

$$\hat{T}_d \mathcal{L}_V \rho^{(S-B)}(t) = \hat{T}_d \mathcal{L}_V \rho_{nd}^{(S-B)}(t), \quad (\text{A.16})$$

we may reduce Eq. (A.11) to

$$\dot{\rho}_d^{(S-B)}(t) = -i\hat{T}_d \mathcal{L}_V \rho_{nd}^{(S-B)}(t), \quad (\text{A.17})$$

where the off-diagonal component is coupled to the diagonal one by the relation

$$\rho_{nd}^{(S-B)}(t) = -i \int_0^t d\tau \mathcal{U}(\tau) \hat{T}_d \mathcal{L}_V \rho_d^{(S-B)}(t - \tau). \quad (\text{A.18})$$

The unitary time-propagation superoperator reads

$$\mathcal{U}(\tau) = \exp \left[-i(\mathcal{L}_0 + \hat{T}_{nd} \mathcal{L}_V) \tau \right]. \quad (\text{A.19})$$

In the case of the considered nonadiabatic ET memory effects are of less importance. We replace in Eq. (A.18) $\rho_d^{(S-B)}(t - \tau)$ by $\rho_d^{(S-B)}(t)$ and extend the time-integral up to infinity. Then, employing relation (A.18) and the asymptotic property (A.1) we end up with the following master-equation:

$$\dot{\rho}_d(t) = -\mathcal{R} \rho_d(t), \quad (\text{A.20})$$

where

$$\mathcal{R} = \int_0^\infty d\tau \text{tr}_{\text{vib}} \left\{ \hat{T}_d \mathcal{L}_V \mathcal{U}(\tau) \hat{T}_{nd} \mathcal{L}_V W_B \right\}, \quad (\text{A.21})$$

is the superoperator which determines the transfer processes.

In order to compute \mathcal{R} we expand $\int_0^\infty d\tau \mathcal{U}(\tau)$ with respect to \mathcal{L}_V . Defining the superoperator $\mathcal{U}^{(0)}(\tau) = \exp(-i\mathcal{L}_0\tau)$ and noting

$$\int_0^\infty d\tau e^{i\omega\tau} \mathcal{U}(\tau) = i \lim_{\varepsilon \rightarrow +0} (\omega - \mathcal{L}_0 - \hat{T}_{nd} \mathcal{L}_V + i\varepsilon)^{-1} \equiv i\mathcal{G}(\omega), \quad (\text{A.22})$$

$$\int_0^\infty d\tau e^{i\omega\tau} \mathcal{U}^{(0)}(\tau) = i \lim_{\varepsilon \rightarrow +0} (\omega - \mathcal{L}_0 + i\varepsilon)^{-1} \equiv i\mathcal{G}^{(0)}(\omega), \quad (\text{A.23})$$

one can see that [61]

$$\begin{aligned} \mathcal{G}(\omega) &= \mathcal{G}^{(0)}(\omega) + \mathcal{G}^{(0)}(\omega) \hat{T}_{nd} \mathcal{L}_V \mathcal{G}^{(0)}(\omega) \\ &\quad + \mathcal{G}^{(0)}(\omega) \hat{T}_{nd} \mathcal{L}_V \mathcal{G}^{(0)}(\omega) \hat{T}_{nd} \mathcal{L}_V \mathcal{G}^{(0)}(\omega) \\ &\quad + \dots \end{aligned} \quad (\text{A.24})$$

Since $\mathcal{G}^{(0)}(0) = \int_0^\infty d\tau \mathcal{U}^{(0)}(\tau)$, we get the expansion

$$\begin{aligned} \int_0^\infty d\tau \mathcal{U}(\tau) &= \int_0^\infty d\tau \mathcal{U}^{(0)}(\tau) + \int_0^\infty d\tau \mathcal{U}^{(1)}(\tau) \\ &\quad + \int_0^\infty d\tau \mathcal{U}^{(2)}(\tau) + \dots, \\ \int_0^\infty d\tau \mathcal{U}^{(n)}(\tau) &= (-i)^n \int_0^\infty d\tau \int_0^\infty d\tau_1 \int_0^\infty d\tau_2 \dots \\ &\quad \times \int_0^\infty d\tau_n \mathcal{U}^{(0)}(\tau) \hat{T}_{nd} \mathcal{L}_V \mathcal{U}^{(0)}(\tau_1) \\ &\quad \times \hat{T}_{nd} \mathcal{L}_V \mathcal{U}^{(0)}(\tau_2) \dots \hat{T}_{nd} \mathcal{L}_V \mathcal{U}^{(0)}(\tau_n). \end{aligned} \quad (\text{A.25})$$

A.2. Kinetic equations for occupation number populations

Let us start from the following linear balance equations:

$$\dot{\mathcal{P}}_a(t) = - \sum_b \langle a | (\mathcal{R} | b \rangle \langle b | | a \rangle \mathcal{P}_b(t), \quad (\text{A.26})$$

for the total electronic populations $\mathcal{P}_a(t)$ of the LWR-system. [In line with definition (A.8) these equations are completely identical to master Eq. (A.20).] Taking into account the fact that for the occupation number representation the many-particle state (A.5) appears as a product of single-particle states $|N_j\rangle$, it is convenient to denote the many-particle population $\mathcal{P}_a(t) = \mathcal{P}_{\{N_j\}}(t)$ as a product of single-particle populations

$$\mathcal{P}_{\{N_j\}}(t) = \prod_{\mathbf{k}} P(N_{L\mathbf{k}}, t) \prod_{\mathbf{q}} P(N_{R\mathbf{q}}, t) \prod_{m=0}^{N+1} P(N_m, t). \quad (\text{A.27})$$

Introducing this ansatz into Eq. (A.26), summarizing both parts of Eq. (A.26) over all occupation numbers except N_j , and utilizing the definition Eq. (A.9) we arrive at the following kinetic equations for the occupation number distributions $P(N_j, t)$

$$\begin{aligned} \dot{P}(N_j, t) = & \sum_{\{N_j''\} \neq N_j} \sum_{\{N_j'\}} \langle \{N_j''\} | (\mathcal{A} | \{N_j'\} \rangle \langle \{N_j'\} |) | \{N_j''\} \rangle \\ & \times \mathcal{P}_{\{N_j'\}}(t). \end{aligned} \quad (\text{A.28})$$

These equations represent master equations written in the occupation number representation. They are of basic importance for the derivation of kinetic equations for the occupation number distributions $P(N_j, t)$ and for the state populations $P_j(t)$. To write down the set of equations (A.28) in a more concrete form one can utilize the expansion Eq. (A.25) and the expression for the Hamiltonian H_0 , Eqs. (A.12), (23) and (19), as well as the interaction V , Eq. (24). Moreover, one also has to take into consideration the following rules specifying the action of the pseudo-spin operators on the occupation number states

$$\sigma_m^- |N_m\rangle = (2N_m - 1) |N_m\rangle, \quad (\text{A.29})$$

$$\sigma_m^+ |N_m\rangle = (1 - N_m) |(1 - N)_m\rangle,$$

$$\sigma_m^- |N_m\rangle = N_m |(1 - N)_m\rangle. \quad (\text{A.30})$$

A.3. Kinetic equations in the Born approximation

In deriving kinetic equations for the wire-internal populations $P_m(t)$, ($m = 1, 2, \dots, N$) one has to notice the restriction on the limit of nonadiabatic transfer. Therefore, we can restrict ourself to the (second) Born approximation with respect to V . We replace $\mathcal{U}(\tau)$ by $\mathcal{U}^{(0)}(\tau)$ in the superoperator Eq. (A.21), and in line with relation Eq. (33) we have to derive an equation for $P(N_m, t)$. It follows from Eq. (A.28) that

$$\begin{aligned} \dot{P}(N_m, t) = & \frac{1}{\hbar^2} \sum_s |V_{ms}|^2 \sum_{N_s} [N_m(1 - N_s) + (1 - N_s)N_m] \\ & \times \{P((1 - N)_m, t)P((1 - N)_s, t)(\mathcal{K}_{sm} + \mathcal{K}_{sm}^*) \\ & - P(N_m, t)P(N_s, t)(\mathcal{K}_{ms} + \mathcal{K}_{ms}^*)\}. \end{aligned} \quad (\text{A.31})$$

The correlation function reads as

$$\mathcal{K}_{ms} = \int_0^\infty d\tau e^{-i(\epsilon_m - \epsilon_s)\tau/\hbar} \text{tr}_{\text{vib}} \left(W_B e^{\hat{R}_{ms}(\tau)} e^{-\hat{R}_{ms}} \right), \quad (\text{A.32})$$

where the ϵ_m are defined by Eq. (1), while

$$\hat{R}_{ms}(\tau) = \exp(-iH_B\tau/\hbar) \hat{R}_{ms} \exp(iH_B\tau/\hbar). \quad (\text{A.33})$$

The concrete form of \hat{R}_{ms} is determined by the used type electron–vibrational coupling. In the case of a local-coupling model, we have $\hat{R}_{ms} = \hat{R}_m - \hat{R}_s$ with \hat{R}_m defined by Eq. (16). When a Holstein model is employed then $\hat{R}_{ms} = \sum_\lambda (g_{m\lambda} - g_{s\lambda})(b_\lambda^+ - b_\lambda)$, ($g_{m\lambda} = \kappa_{m\lambda}/\hbar\omega_\lambda$).

According to the relations Eq. (33) it becomes possible to derive the following kinetic equation for the population $P_m(t)$ of the m th site:

$$\begin{aligned} \dot{P}_m(t) = & -\frac{2\pi}{\hbar} \sum_s |V_{ms}|^2 \{P_m(t)(1 - P_s(t))(\text{FC})_{ms} \\ & - (1 - P_m(t))P_s(t)(\text{FC})_{sm}\}. \end{aligned} \quad (\text{A.34})$$

Here, we introduced the Franck–Condon factor $(\text{FC})_{ms}$ (as well as $(\text{FC})_{sm}$) which has been obtained as a result of the averaging of the operators H_B , Eq. (19) and \hat{R}_{ms} , Eq. (16) with respect to the vibrational states. It follows the standard expression

$$(\text{FC})_{ms} = \frac{1}{2\pi\hbar} \int_{-\infty}^{+\infty} d\tau e^{-i(\epsilon_m - \epsilon_s)\tau/\hbar} e^{-Q_{ms}(\tau)}, \quad (\text{A.35})$$

where the function

$$\begin{aligned} Q_{ms}(\tau) = & 2 \int_{-\infty}^{+\infty} \frac{d\omega}{\omega^2} J_{ms}(\omega) \left[\coth \frac{\hbar\omega}{k_B T} (1 - \cos\omega\tau) \right. \\ & \left. - i \sin\omega\tau \right], \end{aligned} \quad (\text{A.36})$$

comprises the influence of the bath vibrational modes on the ET via the vibrational spectral density $J_{ms}(\omega)$. (This quantity is of basic importance for any calculation done on the spin-boson model [3,5,6,61].) If the transition $m \rightarrow s$ is accompanied by the coupling to a single vibration with frequency ω_f one can utilize the Song–Marcus model [64], where we have $J_{ms} = (1/2\hbar)E_f^{(r)}\omega\delta(\omega - \omega_f)$ and where $E_f^{(r)}$ denotes the reorganization energy for the $m \rightarrow s$ ET. As it well-known the Song–Marcus model leads to Jortner’s form of the Franck–Condon factor [63]

$$(\text{FC})_{ms} = \frac{1}{\hbar\omega_f} \Phi_{v_f}. \quad (\text{A.37})$$

Here, we introduced

$$\begin{aligned} \Phi_{v_f} = & \exp \left[-S_f \coth \frac{\hbar\omega_f}{k_B T} \right] \left(\frac{1 + n(\omega_f)}{n(\omega_f)} \right)^{v_f/2} \\ & \times I_{v_f} \left(2S_f [n(\omega_f)(1 + n(\omega_f))]^{1/2} \right). \end{aligned} \quad (\text{A.38})$$

The expression contains the modified Bessel function $I_\nu(z)$, the Bose distribution function $n(\omega) = [\exp(\hbar\omega/k_B T) - 1]^{-1}$, and we have set $S_f \equiv E_f^{(r)}/\hbar\omega_f$. The energy $E_f^{(r)}$ is the above mentioned reorganization energy of the f th transition caused by the driving force ΔE_f , and $v_f \equiv \Delta E_f/\hbar\omega_f$. For instance, at $m = 1, s = 0$ we put $E_f^{(r)} = E_1^{(r)}$, $\Delta E_f = \Delta E_1 = \epsilon_1 - \epsilon_0$, $\omega_f = \omega_1$, $v_f = v_1$.

The derived kinetic equations (A.34) depend nonlinearly on the site populations. However, it can be guaranteed for the reactions studied in the present paper that the wire-internal units are less populated during the ET process, i.e.

$$P_m(t) \ll 1, \quad (m = 1, 2, \dots, N), \quad (\text{A.39})$$

is fulfilled at any time t . Resulting from this property a reduction to linear balance-like equations

$$\dot{P}_m(t) = - \sum_s [k_{ms}P_m(t) - k_{sm}P_s(t)], \quad (\text{A.40})$$

becomes possible. Here, each rate constant is defined as

$$k_{ms} = \frac{2\pi}{\hbar} |V_{ms}|^2 (\text{FC})_{ms}, \quad (\text{A.41})$$

with the Franck–Condon factor given by Eq. (A.35). A similar Born approximation results in a nonlinear kinetic equation valid for the population of the \mathbf{k} th level of the left-electrode conduction band

$$\begin{aligned} \dot{P}_{\mathbf{Lk}}(t) = & -\frac{2\pi}{\hbar} |V_{\mathbf{Lk}}|^2 [P_{\mathbf{Lk}}(t)(1 - P_0(t))(\text{FC})_{\mathbf{Lk}0} \\ & - (1 - P_{\mathbf{Lk}}(t))P_0(t)(\text{FC})_{0\mathbf{Lk}}]. \end{aligned} \quad (\text{A.42})$$

The Franck–Condon factors are defined via the above given general expression Eqs. (A.35) and (A.36), where now $m = \mathbf{Lk}$, $s = 0$ or $m = 0$, $s = \mathbf{Lk}$. Correspondingly, we obtain

$$(\text{FC})_{\mathbf{Lk}0} = \frac{1}{2\pi\hbar} \int_{-\infty}^{+\infty} d\tau e^{-i(E_{\mathbf{Lk}} - \epsilon_0)\tau/\hbar} e^{-Q_0(\tau)}. \quad (\text{A.43})$$

The function $Q_0(\tau)$ is defined by Eq. (A.36) through the spectral density $J_0(\omega)$. The only difference to $Q_{ms}(\tau)$ results from the fact that during the wire-internal ET $J_{ms}(\omega)$ is defined by the vibrations related to the two sites, m and s , while for electrode–site or site–electrode transition the vibrations are relate to a single site, $m = 0$ ($m = N + 1$ for a right electrode).

Let us sum up Eq. (A.42) with respect to \mathbf{k} and bearing in mind that the total number of electrons occupying the conducting band of the left electrode is $N_L(t)$, Eq. (27). For a bulk electrode, $N_L(t)$ is given by a macroscopic large number. Practically, it does not change during the electron motion through the molecular wire. Therefore, we may set

$$N_L(t) \simeq N_L = \sum_{\mathbf{k}} f_{\mathbf{Lk}}, \quad (\text{A.44})$$

where $f_{\mathbf{Lk}} = \{\exp[(E_{\mathbf{Lk}} - E_F)/k_B T] + 1\}^{-1}$ is the equilibrium Fermi distribution function for the left electrode. According to Eq. (A.44) one can replace in the right part of Eq. (A.42) the population $P_{\mathbf{Lk}}(t)$ by the equilibrium distribution $f_{\mathbf{Lk}}$ once the summation of Eq. (A.42) over \mathbf{k} has been carried out. This treatment leads us to the first equation of the set of equations (36) with the rate constants

$$\begin{aligned} \chi_L &= \frac{2\pi}{\hbar} \sum_{\mathbf{k}} |V_{\mathbf{Lk}}|^2 f_{\mathbf{Lk}} (\text{FC})_{\mathbf{Lk}0}, \\ \chi_{-L} &= \frac{2\pi}{\hbar} \sum_{\mathbf{k}} |V_{\mathbf{Lk}}|^2 (1 - f_{\mathbf{Lk}}) (\text{FC})_{0\mathbf{Lk}}. \end{aligned} \quad (\text{A.45})$$

Analogously, one derives the last equation of set (36). The form of corresponding rate constants, χ_R and χ_{-R} , follows from Eq. (A.45) replacing the symbol \mathbf{Lk} by \mathbf{Rq} .

A.4. Formation of a superexchange transfer rate between the terminal wire units

In the considered model of ET through a molecular wire the terminal wire units 0 and $N + 1$ act as a donor and an acceptor with respect to internal wire units. Therefore, the terminal units do not only couple to the adjacent electrodes and the neighboring wire units but also one to another through the bridging sites $m = 1, 2, \dots, N$. To derive the rate constants $k_1 \equiv k_{0N+1}$ and $k_2 \equiv k_{N+10}$ which include the distant superexchange coupling between the sites 0 and $N + 1$ one has to consider higher orders of perturbation theory with respect to the interaction V . Our aim is to derive a kinetic equation for the population $P_0(t)$ starting from the basic master Eq. (A.28). For the computation of the superoperator \mathcal{R} responsible for the ET we utilize the expansion (A.25) and keep the necessary number of terms to couple site 0 to site $N + 1$. The Born approximation results in kinetic processes which couple site 0 to the left electrode (with rate constants χ_L and χ_{-L}) and to site 1 (with rate constants $\alpha_0 \equiv k_{01}$ and $\beta_0 \equiv k_{10}$). [Details on the formation of these processes are given in the previous subsection.]

Since the interaction V is off-diagonal with respect to the electronic states, the first nonvanishing contribution following the second-order contribution stems from the time-propagation superoperator $\mathcal{U}^{(2)}(\tau)$. This contribution leads to two different contributions, a renormalization of the rate constants (χ_L , χ_{-L} , α_0 and β_0), and transitions between the sites 0 and 2 (with rates k_{02} and k_{20}). Since nonadiabatic ET is considered the intersite matrix elements $V_{mm\pm 1}$ are small. Therefore, we can omit the rate constant renormalization. The rates expressions k_{02} and k_{20} are of the type of superexchange ET rates. But, if the number of internal wire units N exceeds 1, then site 2 belongs to the bridging units. Due to the large gap $\epsilon_2 - \epsilon_0$ between bridging site 0 and 2 the rates k_{02} and k_{20} become too small to have any significant influence on the ET process (more details with respect to this question can be found in [51]). Of course, if the wire has only a single bridging unit one can not ignore the rates k_{02} and k_{20} .

To determine the superexchange rates k_{02} and k_{20} at $N = 1$ one has to expand Eq. (A.28) with \mathcal{R} defined by $\mathcal{U}(\tau) = \mathcal{U}^{(2)}(\tau)$. There are a number of different terms which specify the superoperator \mathcal{R} , each of them contains the integration over τ , τ_1 and τ_2 . Let us consider a typical integral

$$\begin{aligned} A = & \frac{1}{\hbar^4} \int_0^\infty d\tau \int_0^\infty d\tau_1 \int_0^\infty d\tau_2 e^{-i(\epsilon_1 - \epsilon_2)\tau_2/\hbar} e^{-i(\epsilon_0 - \epsilon_2)\tau_1/\hbar} \\ & \times e^{-i(\epsilon_0 - \epsilon_1)\tau/\hbar} \text{tr}_{\text{vib}} \left\{ W_B \tilde{V}_{01}(\tau + \tau_1) \tilde{V}_{21}(\tau) \tilde{V}_{10}(0) \right. \\ & \left. \times \tilde{V}_{12}(\tau + \tau_1 + \tau_2) \right\}, \end{aligned} \quad (\text{A.46})$$

where we introduced $\tilde{V}_{mm'}(\tau) = V_{mm'} \exp(-iH_B\tau/\hbar) \exp(\hat{R}_{mm'}) \exp(iH_B\tau/\hbar)$. It follows from the structure of the integrand that its oscillatory contributions are defined by the factors that contain the energy gaps $\Delta\epsilon_{12} = \epsilon_1 - \epsilon_2$, $\Delta\epsilon_{02} = \epsilon_0 - \epsilon_2$ and $\Delta\epsilon_{10} = \epsilon_1 - \epsilon_0$. The relation provide that at $N = 1$ just the energy ϵ_1 characterizes the position of the bridging LUMO-level. In line with the condition for deep tunneling one has to suppose the validity of the inequalities $\Delta\epsilon_{10} \gg |\Delta\epsilon_{02}|$ and $\Delta\epsilon_{12} \gg |\Delta\epsilon_{02}|$. Following from this the characteristic oscillation time $\tau_1 \sim \hbar/\Delta\epsilon_{02}$ strongly exceeds the characteristic times $\tau \sim \hbar/\Delta\epsilon_{10}$ and $\tau_2 \sim \hbar/\Delta\epsilon_{12}$. This circumstance allows us to omit the times τ and τ_2 in the interactions $\tilde{V}_{01}(\tau + \tau_1)$, $\tilde{V}_{21}(\tau)$ and $\tilde{V}_{12}(\tau + \tau_1 + \tau_2)$. Noting that $\int_0^\infty d\tau \exp(-i\tau x) = -i \lim_{\delta \rightarrow +0} (x - i\delta)$ and thus $\int_0^\infty d\tau \exp(i\Delta\epsilon_{10}\tau) \int_0^\infty d\tau_2 \exp(-i\Delta\epsilon_{12}\tau) \approx \hbar^2/(\Delta\epsilon_{10}\Delta\epsilon_{12})$ the integral Eq. (A.46) is reduced to

$$A \approx \frac{1}{\hbar^2} \frac{|V_{01}V_{12}|^2}{\Delta\epsilon_{10}\Delta\epsilon_{12}} \mathcal{K}_{02}, \quad (\text{A.47})$$

where the correlation function is defined by Eq. (A.32). The multiple time-integrals in the other terms contributing to the expansion have an analogous structure. Collecting all contributions it results a kinetic equation for $P_0(t)$ which is represented as a second equation in the set (36) with the superexchange rate constants

$$k_{1(2)} \equiv k_{02(20)} = \frac{2\pi}{\hbar} \frac{|V_{01}V_{12}|^2}{\Delta\epsilon_{10}\Delta\epsilon_{12}} (\text{FC})_{02(20)}. \quad (\text{A.48})$$

At large numbers N of internal wire units one has to take into consideration the superoperators $\mathcal{U}^{(4)}(\tau)$, $\mathcal{U}^{(6)}(\tau)$ and so on. The superoperator $\mathcal{U}^{(4)}(\tau)$ leads to a renormalization of the previously discussed rates $k_{01(10)}$ as well as $k_{02(20)}$, and generates the formation of the superexchange rate constants k_{03} and k_{30} . But again, if site 3 belongs to a bridge we can neglect the kinetic processes characterized by the rate constants k_{03} and k_{30} . Thus, one can omit the contribution of the superoperator $\mathcal{U}^{(4)}(\tau)$. Generally, one can neglect the contribution from any superoperator $\mathcal{U}^{(2(m-1))}(\tau)$, since it couples site 0 to any internal wire site $m = 2, 3, \dots, N$. However, for $m = N + 1$ we have to consider the respective contribution since we arrived at the superoperator $\mathcal{U}^{(2N)}(\tau)$ which is responsible for the formation of the superexchange transfer process between the 0th and the $N + 1$ th terminal sites.

Thus, to derive the kinetic equations for $P(N_0, t)$ for the case of large energy gaps

$$\Delta\epsilon_{m0} \equiv \epsilon_m - \epsilon_0, \quad \Delta\epsilon_{mN+1} \equiv \epsilon_m - \epsilon_{N+1}, \quad (\text{A.49})$$

between the LUMO-levels of internal and terminal wire units, it is quite appropriate to only keep in the expansion (A.25) the superoperators $\mathcal{U}^{(0)}(\tau)$ and $\mathcal{U}^{(2N)}(\tau)$. This results in the second equation of set (36) with rate expressions

$$k_{1(2)} = \frac{2\pi}{\hbar} |V_{0N+1}|^2 (\text{FC})_{0N+1(N+10)}. \quad (\text{A.50})$$

Here, the square of the superexchange coupling reads

$$|V_{0N+1}|^2 = \frac{|V_1 V_B^{N-1} V_N|^2}{\prod_{m=1}^N \Delta\epsilon_{m0} \Delta\epsilon_{mN+1}}, \quad (\text{A.51})$$

while the Franck–Condon factors coincide with those given in Eq. (A.35) for $m = 0$, $s = N + 1$ or $m = N + 1$, $s = 0$. Note that Eq. (A.50) for the rate constants is valid if the condition

$$|V_{mm\pm 1}| \ll \Delta\epsilon_{m0}, \Delta\epsilon_{mN+1}, \quad (\text{A.52})$$

of deep tunneling is valid for all internal wire units $m = 1, 2, \dots, N$. Take also into account that the superexchange coupling $|V_{0N+1}|$ depends on the applied voltage V through the gaps $\Delta\epsilon_{m0}$ and $\Delta\epsilon_{mN+1}$. If, however, the voltage does not essentially alternate the gaps one can set $\Delta\epsilon_{10} \approx \Delta\epsilon_{20} \approx \dots \Delta\epsilon_{N0} \equiv \Delta E_0$, $\Delta\epsilon_{1N+1} \approx \Delta\epsilon_{2N+1} \approx \Delta\epsilon_{NN+1} \equiv \Delta E_{N+1}$. This leads to the simplified form of the superexchange coupling so that we may set

$$|V_{0N+1}|^2 \approx \frac{|V_1 V_N|^2}{\Delta E_0 \Delta E_{N+1}} e^{-\zeta(N-1)}, \quad (\text{A.53})$$

where the diminishing constant ζ is defined by Eq. (64).

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