## **Designing Smart Particles for the Assembly of Complex Macroscopic Structures**\*\*

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## In memory of Jon Weaver

The development of modern technologies, from tissue engineering to catalysis or energy storage, requires novel lightweight structures combining optimum mechanical and functional response.<sup>[1-4]</sup> This demand is driving the development of new manufacturing techniques to build materials with complex shapes and architectures exhibiting characteristic features from the nanoscopic level and up. Ideally, these techniques should be flexible, remain low-cost and enable high-volume fabrication. A very attractive alternative is the use of wet processing technologies based on smart particles that are able to assemble in response to external stimuli. Ideally, the assembly process should be reversible and programmable, allowing an effective manipulation of the strength of particle-particle interactions. However, the design of responsive particles to build complex meso- to macroscopic structures starting from assembly at the nano- to microscale is very challenging, and today its use is limited mostly to nanostructures and coatings.<sup>[5,6]</sup>

Herein we describe a novel manufacturing process to fabricate macroscopic inorganic structures with complex architectures based on the design of responsive particle surfaces. The method uses a pH-responsive branched copolymer surfactant (BCS)<sup>[7–9]</sup> to functionalize the surfaces in situ and create smart inorganic particles that can self-disperse or assemble between themselves or with soft templates (that is, in emulsified suspensions) under the action of an external trigger (pH). The process allows the fabrication of strong materials with complex shapes, and a wide range of micro- to macroscale architectures from dense to foams with closed or open cells or even graded structures (Figure 1). The method does not depend on the particle chemistry but on the interactions between the BCS molecules functionalizing the

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Figure 1. A) BCS structure showing the branch functionalities. B) pHtriggered assembly of an oil-in-water emulsified suspension of BCSfunctionalized ceramic particles. C) The BCS-particle-droplet and BCS-particle interactions. D) Evolution of the viscoelastic (G', G") properties of an emulsified suspension with changing pH, illustrating the assembly process. Particles and droplets are initially steric and electrostatically stabilized at high pH, the MAA branches are in their anionic form, and the hydrogen bonds are switched off. When the pH value drops below 5 (longer times), the MA branches are completely protonated (hydrogen bonds switched on) and the functionalized particles and droplets (B) bond, forming a network; G' (filled symbols) and G" (open symbols) reach values above 20 kPa. E,F) Examples of ceramic structures fabricated through responsive self-assembly: E) porous SiC from an emulsion and F) sintered highly dense (>99% of the theoretical value) alumina obtained from a suspension (fourpoint bending strength,  $200 \pm 50$  MPa).

surfaces, and herein we use  $Al_2O_3$  and SiC to illustrate its versatility.

The BCS is based on methyl methacrylic acid (MAA) and polyethylene glycol methacrylate (PEGMA) with hydrophobic dodecanethiol (DDT) chain ends and ethylene glycol di-methacrylate (EGDMA) as cross linker (Figure 1A).<sup>[7-9]</sup> This amphiphilic molecule can segregate to oil–water interfaces and stabilize them.<sup>[9]</sup> Furthermore, the branched architecture ensures that each molecule contains multiple poten-

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tial points of attachment to the surface of an inorganic particle to functionalize it and promote its segregation to oil-water interfaces<sup>[10]</sup> in an emulsion (Figure 1B,C). Attachment and functionalization occurs by the following mechanisms: 1) The interactions of the hydrophobic chain ends (DDT) on the surfaces; 2) the electrostatic interaction between the carboxylic anions in the MAA residues (COO<sup>-</sup>) with the positively charged particle surfaces; and 3) the establishment of chemical covalent bonding between the carboxylic residues and the metal oxides on the surface of the particles (Figure 1).<sup>[11,12]</sup>

The process starts with the BCS functionalization of the inorganic particles in concentrated water-based suspensions (for details, see the Supporting Information). Analysis of these suspensions by dynamic light scattering (DLS) and inducted coupled spectroscopy (ICP) shows that for particles with sizes of the order of 200-500 nm the optimum BCS concentration ranges between 1 and 2 % wt/v (with regards to volume of suspension). At these BCS concentrations the particles are well-dispersed, and ICP analyses of the sulfur concentrations in the liquid indicate that 26% of BCS molecules are attached to the particles, while 74% remain in solution. At basic pH (8-12), the functionalities in the branches (EG and MAA) provide steric and electrostatic stabilization, allowing the formulation of well-dispersed colloidal suspensions that can reach very high solid contents (up to 60 vol%). If needed for the fabrication of complex structures, these colloidal suspensions can be easily emulsified with decane (50-60 vol % related to the suspension volume). The oil droplets are stabilized by a synergetic combination of the BCS molecules in the liquid and the functionalized particles, both of which attach to the oil-water interface (Figure 1 B,C). Particles with wetting angles of the order of 70° attach irreversibly to the oil-water interface with higher energy than usually observed for surfactant molecules.<sup>[13,14]</sup> In this respect, functionalization with BCS modifies the wettability of the ceramic particle surfaces increasing the water contact angle (Supporting Information, Figure S3).<sup>[15-18]</sup> Particle-BCS stabilized emulsions can be stored without destabilization for more than 1 month. These stable droplets act as a temporary soft template for the fabrication of porous structures (Figure 1E).

At high pH, both suspensions and emulsions are very fluid (with viscosities between 0.02-0.04 Pa). However, under acidic conditions (below the apparent  $pK_a$  of the MAA residues,  $pK_a \approx 5$ ) the BCS-functionalized surfaces "turn on" multiple links between the molecules, functionalizing particles and droplets as the neutral MAA residues form hydrogen bonds with the EG residues (Figure 1B). In this way, a pH switch triggers a self-assembly process to form in situ solid parts that can be easily handled and retain the complex shape of the mold. Subsequently these parts can be dried and sintered to form fully inorganic structures that can be dense (from suspensions) or porous (from emulsions) with a wide range of architectures depending on the degree of emulsification, the properties of the starting suspension, the kinetics of the self-assembly and the solvent evaporation rate. The variables that affect the kinetics and strength of the assembly are temperature, relative concentration of BCS, solid loading, and amount of the pH regulator (herein we used glucono- $\delta$ -lactone, G $\delta$ L, the hydrolysis of which to gluconic acid is used to homogeneously decrease in pH).

As the pH decreases, the dispersed-to-aggregated phase transition can be divided in three stages: I) early stage assembly, II) network formation, and III) plateau (Figure 1D). During the early stage, a weak gel network is established; the crossover point that indicates gel formation (where the viscoelastic properties, storage (G') and loss (G'')moduli reach the same value) takes place shortly after triggering the pH drop. As the pH decreases, more links between particles and droplets are turned on and the gel becomes rapidly a stiff network (stage II, Figure 1D). During the third stage, the moduli reach a plateau where the formation of multiple hydrogen bonds creates a strong particle network. Larger BCS concentrations lead to longer aggregation times, which is due to its buffer role while higher particle concentrations result in the faster formation of stronger materials, as in diluted suspensions the long distance between particles results in slower aggregation and a weaker particle network. We can easily reverse the assembly process by switching off the hydrogen bonds in the networks by, for example, submerging the structures in alkaline aqueous solution (pH12; Figure 2A). The structures disassemble into dispersed particles and droplets owing to hydrogen-



Figure 2. A) Reversible aggregation of a complex-shaped porous structure obtained by emulsion templating (left); de-aggregation of the particle/droplet network in alkaline water (middle); ceramic suspension recovered after "turning off" the hydrogen bonds (right). B) Compressive strength of the cellular  $\mathsf{Al}_2\mathsf{O}_3$  ceramics synthesized herein compared with reported data for porous alumina foams.[17, 19-30] The theoretical predictions from the Gibson and Ashby model are included for comparison (dashed lines; considering a three-point bending strength of 400 MPa for dense counterparts;  $\phi$  is the fraction of solids in cell faces, 0=closed cell, 1=open cell).<sup>[31]</sup> C),D) Corresponding microstructures: C) closed-cell Al<sub>2</sub>O<sub>3</sub> (porosity ca. 55%) obtained from a suspension containing 43 vol% of particles in BCS solution (1% wt/ v, pH 8) emulsified with 50 vol% decane at 2000 rpm; D) alumina structure with highly interconnected porosity (porosity ca. 80%) obtained from a suspension containing 15 vol% of particles homogenized with 50 vol% decane at 24000 rpm. Higher emulsification speeds lead to a finer interconnected porosity.

bond decomplexation and electrostatic repulsion of the anionic MAA residues on the droplet and particle surfaces.

The self-assembly of particles and soft templates provides an excellent route to tune the architecture of cellular ceramics. By manipulating the emulsification conditions (solid content of the starting suspension, amount of decane used to emulsify and emulsification speed; see the Supporting Information) and the relative kinetics of self-assembly and drying, we can manufacture cellular ceramics with complex shapes and a broad range of microstructures ranging from closed-cell to highly interconnected open porosity (Figure 2 C,D) or structures exhibiting graded architectures, from dense to highly porous (Figure 3). For example, we



**Figure 3.** A) SEM image of a sample with graded porosity. B),C) Structure formed from a 12 vol% alumina suspension emulsified with 50 vol% of decane and subjected to slow-rate solvent elimination: B) Detail of a strut between adjacent pores formed following the plateau border between decane droplets. The sample has not yet been sintered and the walls between pores resulting from the emulsion lamellae are about 500 nm thick. The bubble behind the strut (arrow) illustrates the efficient packing of droplets. C) Honeycomb structure obtained after sintering the material in (B).

have prepared closed-cell cellular ceramics with 50-60% porosity (average size  $30 \mu$ m), and a proportion of open pores below 1-2% or homogeneous and highly porous cellular materials with 80-90% porosity (average size  $15 \mu$ m with a narrow size distribution between 9 and  $30 \mu$ m) in which up to 72% is interconnected and open (Figure 2).

These porous materials exhibit high compressive strengths that in the case of close-cell ceramics can be more than double of those previously reported for similar macroporous ceram- $\mathrm{ics}^{[17,\,19\text{--}30]}$  and could be even above the predictions of the Gibson and Ashby model<sup>[31]</sup> (Figure 2B). This extraordinary mechanical performance reflects the meso- to macroscale structure of the materials and the efficiency of the process. The low viscosity, stability, and wide droplet size distribution of the emulsions (from 10 µm to 80 µm) allow an efficient packing of the oil droplets before assembly and the formation of a remarkably homogeneous 3D architecture. As a consequence, the final pores are not monodisperse, which may explain the deviations from the Gibson and Ashby model.[31] Moreover, the establishment of a strong particle network through the assembly process combined with the very low organic content of the suspension and the use of a soft template help to preserve the integrity of the inorganic part during drying and sintering and enables the formation of dense, defect-free walls (Figure 2 C).

Graded porous structures (Figure 3A) can be created by emulsifying suspensions with low solid loading (7–15 vol%) at moderate stirring speeds (2000 rpm) to create emulsions with limited stability and wide droplet size distributions. The destabilization leads to the formation of a dense layer at the bottom while the oil droplets arrange hierarchically above it, owing to the different densities of oil and water. By tuning the assembly and destabilization kinetics, for example by using relatively high amounts of G $\delta$ L (12–15% wt/v), it is possible to freeze this hierarchical arrangement (small and stable droplets at the bottom and larger and less stable droplets at the top) to form scaffolds with graded porosity (Figure 3A). Moreover, the pore shape of highly porous scaffolds can also be controlled from spherical to polyhedral (Figure 3B,C) by manipulating the solvent evaporation rate. Long drying times enable lamella formation between adjacent oil droplets (Figure 3B), which leads to characteristic polyhedral shapes and highly porous (70-80%) cellular ceramics with very thin walls ( $\leq 1 \,\mu m$ ) after sintering (Supporting Information, Figure S4).

In summary, we have formulated a new approach for the synthesis of smart particles that are able to assemble in response to an external stimulus. These particles can be used in the bottom-up manufacture macroscopic inorganic structures with complex shapes and architectures. The method is independent of the particle chemistry, is versatile, reversible and simple, using surface functionalization with small additions of a single polymer to enable dispersion and trigger assembly. The rheological response of the suspensions can be manipulated to support a range of manufacturing techniques including the formulation of injectable ceramic inks for solid free-form fabrication or injection molding (Supporting Information, Figure S4). The process addresses two standing issues in the fabrication of highly porous materials: how to reliably form them into complex shapes, and how to increase strength, opening new paths for the fabrication of lightweight structural components. The potential for application is very broad including light filters, ceramic films with graded porosity, bulk thermal shock-resistant structures, thermal barrier coatings, or temperature control membranes for automatic thermal reforming, to mention a few. In particular, current research in our group is focusing on the use of closed-cell ceramics as lightweight thermal insulators with structural capabilities and the application of open cell structures as catalytic supports and tissue engineering scaffolds.

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