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# Symmetry and curvature effects on spin waves in vortex-state hexagonal nanotubes

Lukas Körber<sup>1,2,\*</sup>, Michael Zimmermann,<sup>3</sup> Sebastian Wintz,<sup>4,5</sup> Simone Finizio<sup>6</sup>, Matthias Kronseder,<sup>3</sup> Dominique Bougeard,<sup>3</sup> Florian Dirnberger<sup>3</sup>, Markus Weigand<sup>5,6</sup>, Jörg Raabe,<sup>4</sup> Jorge A. Otálora,<sup>7</sup> Helmut Schultheiss,<sup>1,2</sup> Elisabeth Josten,<sup>8</sup> Jürgen Lindner,<sup>1</sup> István Kézsmárki,<sup>9</sup> Christian H. Back,<sup>10,3</sup> and Attila Kákay<sup>1</sup>

<sup>1</sup>*Helmholtz-Zentrum Dresden-Rossendorf, Institute of Ion Beam Physics and Materials Research, Bautzner Landstraße 400, 01328 Dresden, Germany*

<sup>2</sup>*Fakultät Physik, Technische Universität Dresden, D-01062 Dresden, Germany*

<sup>3</sup>*Fakultät für Physik, Universität Regensburg, Universitätsstraße 31, D-93053 Regensburg, Germany*

<sup>4</sup>*Swiss Light Source, Paul Scherrer Institut, 5232 Villigen PSI, Switzerland*

<sup>5</sup>*Max-Planck-Institut für Intelligente Systeme, 70569 Stuttgart, Germany*

<sup>6</sup>*Helmholtz-Zentrum Berlin, 12489 Berlin, Germany*

<sup>7</sup>*Departamento de Física, Universidad Católica del Norte, Avenida Angamos 0610, Casilla 1280, Antofagasta, Chile*

<sup>8</sup>*Ernst Ruska-Centre for Microscopy and Spectroscopy with Electrons (ER-C) and Peter Grünberg Institute (PGI), Forschungszentrum Jülich, 52425 Jülich, Germany*

<sup>9</sup>*Experimental Physics V, University of Augsburg, 86135 Augsburg, Germany*

<sup>10</sup>*Physik-Department, Technische Universität München, 85748 Garching bei München, Germany*



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Analytic and numerical studies on curved magnetic nano-objects predict numerous exciting effects that can be referred to as magneto-chiral effects, which do not originate from intrinsic Dzyaloshinskii-Moriya interaction or interface-induced anisotropies. In contrast, these chiral effects stem from isotropic exchange or dipole-dipole interaction, present in all magnetic materials, which acquire asymmetric contributions in case of curved geometry of the specimen. As a result, for example, the spin-wave dispersion in round magnetic nanotubes becomes asymmetric; namely, spin waves of the same frequency propagating in opposite directions along the nanotube exhibit different wavelengths. Here, using time-resolved scanning transmission x-ray microscopy experiments, standard micromagnetic simulations, and a dynamic-matrix approach, we show that the spin-wave spectrum undergoes additional drastic changes when transitioning from a continuous to a discrete rotational symmetry, i.e., from round to hexagonal nanotubes, which are much easier to fabricate. The polygonal shape introduces localization of the modes to both the sharp, highly curved corners and flat edges. Moreover, due to the discrete rotational symmetry, the degenerate nature of the modes with azimuthal wave vectors known from round tubes is partly lifted, resulting in singlet and duplet modes. For comparison with our experiments, we calculate the microwave absorption from the numerically obtained mode profiles, which shows that a dedicated antenna design is paramount for magnonic applications in 3D nanostructures. To our knowledge these are the first experiments directly showing real space spin-wave propagation in 3D nano-objects.

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## I. INTRODUCTION

After having been proposed by Bloch in the 1930s [1], the propagation of spin waves (SWs)—the elementary excitations in magnetically ordered systems—has been studied extensively. Because of their peculiar linear and nonlinear characteristics, SWs promise great potential in information transport and processing such as the magnon transistor [2] and the magnonic diode [3] for multifunctional spin-wave logic applications. Spin waves (including the spatially uniform ferromagnetic resonance precession) have also been proven to be an excellent tool to probe the magnetic characteristics of solids as they are sensitive to spin currents [4–6], impurities [7–9], crystal anisotropies [10], or asymmetric ex-

change interactions, among others. For example, the presence of an asymmetric interaction such as the Dzyaloshinskii-Moriya interaction (DMI) leads to an asymmetric dispersion and consequently to a nonreciprocal propagation of spin waves therein [11–21]. Similar nonreciprocal spin-wave propagation is observed in magnetic bilayers [22–24]. Therefore, the study of spin-wave propagation is of both a technological as well as a fundamental interest.

While many of the aforementioned effects have been investigated mostly in bulk or in flat thin-film samples, over the last decade, curvature-induced effects have been uncovered as a new way to manipulate magnetic equilibria and spin dynamics. Numerous analytic and numerical works have already shown that the surface curvature and geometry of 3D magnetic membranes leads to phenomena not present in flat specimens of the same material [25–34]. For example, in conventional soft magnetic materials, exotic noncollinear

\*l.koerber@hzdr.de

magnetic textures such as skyrmions [35] may be stabilized by bending the magnetic material. Moreover, magnetization dynamics can be influenced, leading to symmetry breaking of domain-wall motion [25,26], asymmetric spin-wave transport [31,36], or the emergence of a topological Berry phase [37]. The influence of curvature on magnetic equilibria has been shown to be mainly due to a renormalization of the magnetic exchange interaction [29,38]. However, as shown in Ref. [38], the long-range dipole-dipole interaction can also lead to chiral symmetry-breaking effects and thus introducing handedness in an intrinsically achiral material. In our recent works Refs. [31,32,39], we predicted that curvature-induced effects, of both dipolar and exchange origin, lead to an asymmetric dispersion of SWs in round magnetic nanotubes being in the helical state.

In this paper we show that magnetization in 3D nano-objects is not only governed by the curvature and topology. At the example of hexagonal nanotubes we present that the discrete rotational symmetry induces drastic changes in the spin-wave spectra. In particular, the mode spectrum is non-trivially split into standing waves (singlets) and running waves (duplets). In the previously investigated round nanotubes, the modes with the same  $k$  but opposite sign of azimuthal quantization index form duplets, except for the uniform mode, which is a singlet. Moreover, in contrast to round magnetic nanotubes, which are extremely difficult to fabricate with sufficiently low damping, we succeeded in fabricating hexagonal nanotubes and preparing them in the vortex magnetic state [40]. This allowed us, for the first time to our best knowledge, to directly image magnetization dynamics in curved 3D nanostructures, using time-resolved scanning transmission x-ray microscopy (TR-STXM) [41–43]. Prior to this work, experimental evidence in curved samples was restricted to equilibrium effects, such as the spiral Landau pattern in bent rectangular elements [44] or the domain wall pinning by a curvature gradient, shown in parabolic stripes [45].

For the quantitative analysis of the experiments, we have conducted an extensive numerical study using standard micromagnetic simulations as well as our recently developed finite-element propagating-wave dynamic-matrix approach [46]. We find that the mode spectrum of vortex-state hexagonal tubes is asymmetric and quite complex in nature. The polygonal shape introduces localization of the modes into the highly curved corners and flat facets. Moreover, the degenerate nature of the modes with azimuthal wave vectors known from round tubes is lifted in the polygonal case, resulting in singlet and duplet modes. The singlet-duplet differentiation is related to the discrete symmetry resulting from the hexagonal cross section of the waveguide housing a vortex magnetic ground state. Using the spin-wave profiles resulting from our eigensolver, we calculated the dispersion relation with the microwave absorption for two different antenna field profiles, a current loop and a stripline antenna. The numerical results show that the stripline antenna used in the TR-STXM experiments excites multiple modes at a fixed frequency, though with different intensity; thus the resulting spin waves propagating in the nanotube form a beating pattern instead of a single wave with a well-defined wavelength. Therefore to measure and eventually exploit the asymmetry of the dispersion a stripline antenna is not satisfactory. Instead,

a proper design of the microwave antenna is needed to couple and thus excite only single modes with well-defined frequency and wavelength.

In Sec. II we briefly discuss the sample fabrication followed by the description of the micromagnetic methods used in the paper, employed both in the time domain and in the frequency domain. The experimentally measured spin-wave propagation together with finite-element micromagnetic simulations is shown in Sec. III. To understand the spin-wave propagation in hexagonal tubes the dispersion relation is discussed in detail, showing the localization of modes and their singlet-duplet nature related to the combined symmetry of the tube geometry and its ground magnetic state. The predicted microwave absorption and its effect on the spin-wave excitation depending on the antenna geometry is discussed to allow for a realistic comparison of the numerical and experimental results. The conclusions of the study and a possible outlook, with suggestions for further experimental investigations, will be discussed last in Sec. IV.

## II. METHODS

In this section we will briefly summarize the numerical as well as the experimental methods, including the sample fabrication involved in the current study.

### A. Sample fabrication and STXM experiments

The nanotube fabrication involves a two-step routine: first, GaAs rods are grown on oxidized Si(111) wafers via molecular-beam epitaxy (MBE) in a III-V MBE using Ga droplets as catalysts. After *in situ* transfer to a metallic MBE chamber in a pressure lower than  $1 \times 10^{-10}$  mbar, the coating layers composed of the permalloy magnetic layer and an Al capping layer to avoid oxidation are deposited at pressures around  $1 \times 10^{-10}$  mbar (base pressure of  $5 \times 10^{-11}$  mbar). The sparsely populated grown nanotubes are mounted with a gas injection system (GIS) at their tip to a nanomanipulator and cut at their bottom with a focused ion beam (FIB). Subsequently the nanotube is placed as desired (again using the GIS) and the tip is cut off by the ion beam, thus removing the tube from the manipulator. Details of the sample preparation are described in Ref. [40]. As a result of the growth-induced easy-plane magnetic anisotropy perpendicular to the symmetry axis, the equilibrium magnetization is a vortex state, as confirmed by STXM measurements [40].

The TR-STXM measurements were performed to directly image the magnetization dynamics in the tubes in hopes of experimentally obtaining the spin-wave dispersion. The time-resolved measurements were mostly performed at the MAXYMUS endstation of BESSY II at Helmholtz-Zentrum Berlin, Germany. The static and low-frequency (up to 6 GHz) measurements have been done at the POLLUX endstation of the PSI, Villigen, Switzerland.

An exemplary scanning-electron-transmission-microscopy image of a hexagonal nanotube, with 250 nm outer diameter, 30 nm thickness, and  $12 \mu\text{m}$  length, used for the measurements is shown in Fig. 1 together with a sketch of the nanotube and its cross-sectional view. The magnetic nanotube

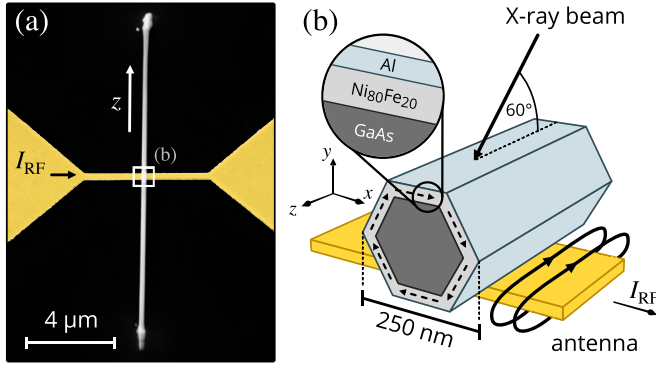


FIG. 1. (a) Scanning-electron-transmission-microscopy image of a hexagonal permalloy nanotube with 250 nm outer diameter, 30 nm thickness, and 12  $\mu\text{m}$  length on a GaAs wire. The gold stripline antenna (here colored for visual purposes) was patterned on a SiN membrane, and the nanotube was placed on the top using a focused ion beam (FIB) tool and a micromanipulator. The Oersted field of an rf current is used to excite SWs. (b) Cross-sectional sketch of the hexagonal nanotube showing the layer structure. The permalloy layer is directly evaporated on the GaAs wire *in situ* and capped with Al to avoid oxidation. A relative angle of 60° was used between the x-ray beam and the symmetry axis of the nanotube. This configuration allows for being sensitive to the in-plane dynamic magnetization of the top and bottom surfaces of the tube, which is expected to be larger than the out-of-plane dynamic magnetization component.

is placed on the top of a gold stripline antenna patterned on a SiN membrane. The nanotube is usually oriented such that one of the flat facets is parallel to the substrate surface, and thus the top facet normal is parallel to the x-ray beam. The absorption images were collected by exploiting the x-ray magnetic circular dichroism (XMCD) effect [47] of the transmitted soft x-ray radiation at the L3 edge of iron (708 eV). The dynamic magnetization contrast to visualize the real space spin-wave propagation was obtained with left circularly polarized light. A Fresnel zone plate is used to focus the x rays to a single spot on the sample, allowing for a lateral resolution of approximately 25 nm when the sample is raster scanned through the beam. The acquired magnetic contrast scales with the projection of the magnetic orientation in the direction of photon propagation. Hence, in normal incidence, our STXM setup is sensitive to the dynamic magnetization component in the propagation direction perpendicular to the top and bottom surfaces. While the 30° inclined sample mounting, compared to the surface normal, used in the experiments also allows for detecting in-plane magnetization components at the same time. To summarize, the photon counts shown in this paper are proportional to the projection of the dynamic magnetization (both in-plane and out-of-plane component) to the direction of the photon beam. The spin waves were excited with the stripline antenna at various frequencies between frequencies of 1 GHz and 10 GHz. Every excitation yielded a seven-frame movie; each frame contains the real-space profiles of the excited spin waves at equidistant phases with respect to the excitation signal. In order to highlight the time-dependent magnetic changes in the sample, a normalized data representation is used where each frame is divided by the time average of all seven frames.

TABLE I. Parameters used for micromagnetic modeling.

|  |                        |
|--|------------------------|
| Exchange stiffness ( $A_{\text{ex}}$ )       | 13 pJ/m                |
| Saturation ( $M_s$ )                         | 820 kA/m               |
| Reduced gyromagnetic ratio ( $\gamma/2\pi$ ) | 28 GHz/T               |
| Gilbert damping ( $\alpha_G$ )               | 0.007                  |
| Uniaxial anisotropy constant ( $K_{u,1}$ )   | $-20 \text{ kJm}^{-3}$ |
| Uniaxial anisotropy direction ( $e_u$ )      | $e_z$                  |
| Tube outer diameter ( $D$ )                  | 250 nm                 |
| Tube shell thickness ( $T$ )                 | 30 nm                  |
| Tube length ( $L$ )                          | 8.0 $\mu\text{m}$      |
| Edge length along tube                       | 5 nm                   |
| Edge length along cross section              | 3 nm                   |

## B. Micromagnetic modeling

In this section we introduce the micromagnetic methods used to investigate the spin-wave propagation and dispersion in our hexagonal nanotubes.

### 1. Finite-element time-domain simulations

In the framework of micromagnetism the magnetization dynamics is described by the Landau-Lifshitz-Gilbert equation of motion,

$$\frac{d\mathbf{m}}{dt} = -\omega_M(\mathbf{m} \times \mathbf{h}_{\text{eff}}) + \alpha_G\left(\mathbf{m} \times \frac{d\mathbf{m}}{dt}\right), \quad (1)$$

where  $\mathbf{m}$  is the reduced magnetization  $\mathbf{m}(\mathbf{r}, t) = \mathbf{M}(\mathbf{r}, t)/M_s$ ,  $M_s$  the saturation magnetization,  $\mathbf{h}_{\text{eff}}$  the normalized effective field,  $\omega_M = \gamma\mu_0 M_s$  the characteristic frequency, and  $\alpha_G$  the Gilbert damping parameter. In order to study the propagation of the spin waves in the hexagonal tubes we have solved numerically the equation of motion using our custom developed GPU accelerated finite-element micromagnetic code TETRAMAG. [48] For the simulations we have considered an 8  $\mu\text{m}$  long hexagonal tube with 30 nm thickness assuming permalloy material parameters. The exact values can be seen in Table I. The equilibrium state, which is a flux-closure state, is computed using a conjugate-gradient energy minimization starting from a circular vortex initial state. The uniaxial anisotropy along the long axis of the tube with a negative constant will prefer a flux-closure (vortex) state. In order to mimic the experimental excitation scheme, monochromatic spin waves were excited at the center of the hexagonal tube using a microwave field of 1.0 mT magnitude, with components in the  $yz$  plane, and with the spatial profile of the field corresponding to the stripline antenna of 250 nm. The rf field with a sinusoidal time variation was applied for 100 periods for all simulated frequencies.

### 2. Propagating-wave dynamic-matrix approach

To numerically calculate the spin-wave dispersion for waves traveling along the hexagonal nanotube we utilize our recently developed finite-element dynamic approach for propagating waves. This approach uses the same spatial discretization method as TETRAMAG [48] and relies on the numerical solution of the eigenvalue problem

$$\frac{\omega_v(k)}{\omega_M} \eta_{vk} = i\mathbf{m}_0 \times \hat{\mathbf{\Omega}}_k \eta_{vk} \quad \text{with} \quad \mathbf{m}_0 \perp \eta_{vk}, \quad (2)$$



which is the nondissipative ( $\alpha_G = 0$ ) version of the LLG equation (1), linearized in the vicinity of some (stable) equilibrium state  $\mathbf{m}_0(\mathbf{r})$  and transformed into a single cross section of the nanotube for the case of plane waves propagating along the  $z$  direction with wave vector  $k$  and angular frequency  $\omega_v(k)$ . Note that the  $z$  axis in this study is the axis along the long axis of the hexagonal nanotube. The eigenvectors  $\boldsymbol{\eta}_{vk} \equiv \boldsymbol{\eta}_{vk}(\boldsymbol{\rho})$  represent the (complex) lateral mode profiles, which depend only on the coordinates  $\boldsymbol{\rho} = (x, y)^T$  and can be denoted additionally by some lateral mode index  $v$  which labels the respective branch of the dispersion.

The plane-wave Hamiltonian operator  $\hat{\Omega}_k$  is given by

$$\hat{\Omega}_k = h_0 \hat{\mathbf{I}} + \hat{\mathbf{N}}_k = h_0 \hat{\mathbf{I}} + e^{-ikz} \hat{\mathbf{N}} e^{ikz} \quad (3)$$

with  $h_0$  being the projection of the unitless static effective field (including any static external field) onto the equilibrium direction,  $\hat{\mathbf{I}}$  the identity operator, and  $\hat{\mathbf{N}}$  the self-adjoint operator describing the magnetic self-interactions, which, in our case, are exchange and dipolar interaction, as well as uniaxial magnetic anisotropy (see Ref. [46]). All operators and vectors are discretized in the framework of the finite-element method. The resulting linear system is numerically diagonalized for each  $k$  value using the iterative Arnoldi-L  nczos method, which yields a desired number of lowest-magnitude eigenvalues  $\omega_v(k)$  as well as their corresponding eigenvectors  $\boldsymbol{\eta}_{vk}$ . In our case, the lowest 30 modes for each  $k$  were calculated for a total number of 201 wave vectors between  $\pm 35$  rad/ $\mu\text{m}$ . To account for the dipolar potential generated by the individual spin-wave modes we employ a modified version of the hybrid FEM/BEM Fredkin-Koehler method, which was recently extended to plane-wave potentials in Ref. [46]. The equilibrium state  $\mathbf{m}_0$  is found by energy minimization, the same way as for the time-domain simulations.

In contrast to a full 3D time-domain simulation, the magnetic nanotube only needs to be modeled in a single cross section which drastically reduces the computational load. The spin-wave frequencies and mode profiles are directly obtained (within minutes), without the need of additional postprocessing. Moreover, as an additional benefit, degenerate modes can be detected, which is not easily possible using a single field pulse followed by an FFT-based analysis.

### III. RESULTS AND DISCUSSION

In this section we will first show the spin-wave propagation measured experimentally using time-resolved STXM and compare it with those from micromagnetic simulations. We would like to emphasize that according to our knowledge these are the first experiments directly showing real space spin-wave propagation in 3D nano-objects.

#### A. Mode localization

To obtain a first overview of the spin-wave transport in hexagonal nanotubes we excite monochromatic waves using a stripline microwave antenna at the center of the tube and at different fixed frequencies.

In Figs. 2(a)–2(d) we show exemplary snapshots of two counter-propagating spin-wave modes at 4.571 GHz, 5.571 GHz, 8.571 GHz and 9.571 GHz, obtained by TR-

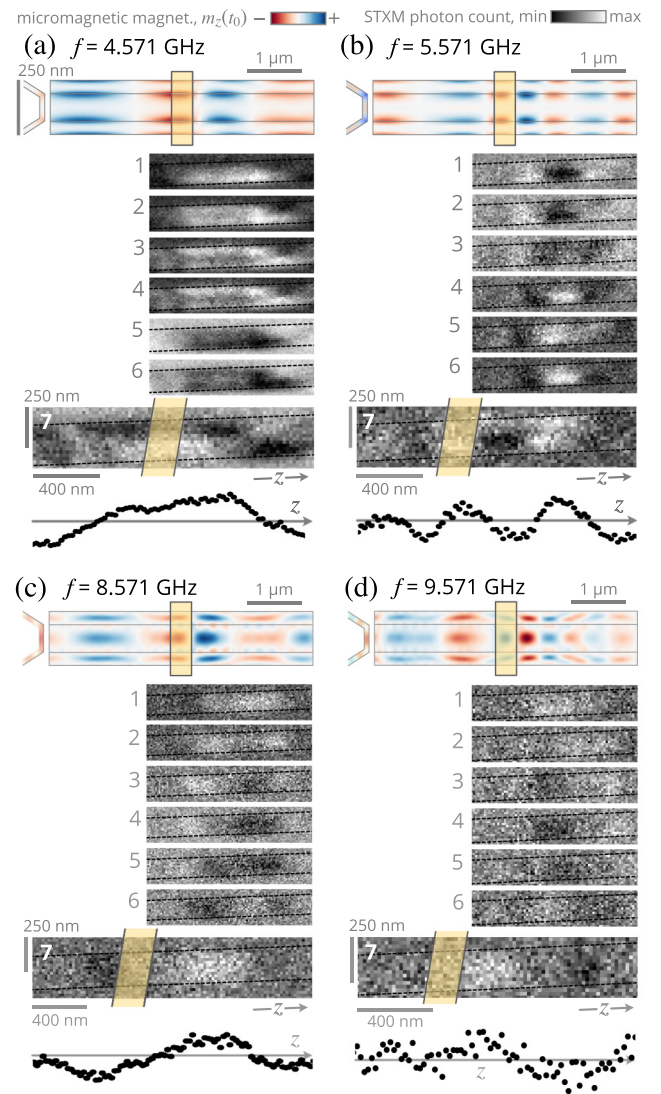


FIG. 2. Numerical (red-blue) and experimental (gray scale) snapshots of the dynamic magnetization at fixed times for modes propagating in the corners of the hexagonal tube (a) at 5.571 GHz and (b) at 4.571 GHz, and for modes mostly propagating in the top and bottom facets (c) at 8.571 GHz and (d) at 9.571 GHz. For the numerical profiles, a side view is shown next to the projection of the upper half the nanotube. For better illustration, they have been stretched in the width direction. Below we show all frames of the respective STXM movies. In addition to each last frame, we show an average line scan along the tube, together with sinusoidal fits used to obtain the wave lengths. The position of the antenna is in all cases marked with a translucent gold-colored patch. The dashed lines in each STXM frame mark approximately the contour of the hexagonal tube.

STXM and time-domain micromagnetic simulation. For the experiments, we show a full oscillation cycle as seven frames. As seen especially from the simulation profiles, the modes exhibit different localization within the cross section of the hexagonal tube, e.g., there are modes more localized in the corners of the tube [5.571 GHz in Fig. 2(a) and 4.571 GHz in Fig. 2(b)] or on the facets of the tube [8.571 GHz and 9.571 GHz in Figs. 2(c) and 2(d)]. We also would like to

refer to the animated experimental movies of these modes, provided in the Supplemental Material [49], which may show the localization of the modes at 4.571 GHz and 5.571 GHz in the corners better than the static frames. We observe an intensity asymmetry of the modes at large frequencies. This is a commonly known effect for Damon-Eshbach SWs (with  $\mathbf{k} \perp \mathbf{m}_0$ ) excited with a stripline antenna in magnetic thin films [50] and is also present here as our tubes are in the vortex state ( $\mathbf{k} \perp \mathbf{m}_0$ ). Moreover, in the numerical mode snapshots at 5.571 GHz [Fig. 2(a)] and 4.571 GHz [Fig. 2(b)], one can already clearly see a wave-vector asymmetry for the two counterpropagating modes, which is the evidence for an asymmetric SW dispersion.

To obtain the wave lengths of the counterpropagating spin waves from the experimental data, we average the measured data for different excitation frequencies along the width of the tube (shown for each last STXM frame in Fig. 2) and fit these curves for individual time frames with decaying sinusoidal functions along the long axis of the tube (propagation direction) on either side of the antenna. Between two and 18 fits could be obtained per frequency and direction. The resulting wave vectors were obtained as the averages of all associated fits. This method was chosen because only a few wavelengths are observed in the measurements, and a Fourier analysis to obtain the wave vectors at a given frequency was not conclusive. Note that from the two-sided fit presented for the corner mode at 5.571 GHz in Fig. 2(a), one can also see a wave-vector asymmetry in the experimental data

### B. Dispersion and mode symmetry

For a more detailed analysis of the modal spectrum, we calculate the full dispersion for all modes below 12 GHz and with wave vectors between  $\pm 35 \text{ rad}/\mu\text{m}$  using the FEM propagating-wave dynamic matrix approach outlined in Sec. II and explained in detail in Ref. [46]. We would like to point out again that, in contrast to usual time-domain simulations based on microwave excitation, this analysis provides access to modes which might have a nontrivial spatial profile and which therefore do not couple to commonly used microwave-field distributions. Moreover, it becomes possible to always separate degenerate modes. The resulting dispersion including all modes is shown in Fig. 3(a). As suggested by the varying mode localization at different excitation frequencies in the previous section, the spectrum is divided into several, in certain cases, even degenerate branches. We will see in the next section that only a few of them are easily accessible in experiments. The different branches  $\nu$  can be categorized by analyzing the corresponding (complex-valued) lateral mode profiles  $\eta_{\nu k}(\rho)$  within the hexagonal-tube cross section. To visualize these, we plot the magnitude  $|\eta_z|$  and the phase  $\arg(\eta_z)$  of the  $z$  component of the mode profiles as color maps in Fig. 3.

As indicated by the magnitudes of the spatial profiles in Fig. 3(b), the branches can be categorized by their localization either to the corners (C) or to the facets (F) of the hexagonal tube. Moreover, there are also several hybrid-corner-facet modes (CF). Apart from their localization, the modes differ in the number of periods along the hexagonal circumference. In this sense, the spin waves in a hexagonal tube are similar

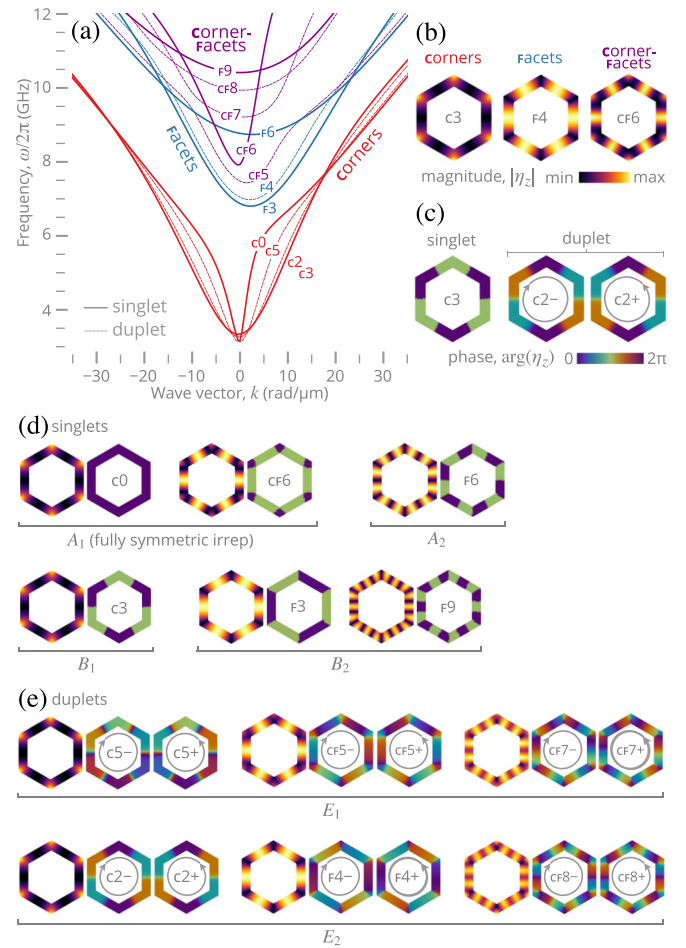


FIG. 3. Dispersion relation and modes profiles directly resulting from the dynamic-matrix approach for propagating spin waves. (a) Full dispersion for all modes below 12 GHz. The modes can be categorized based on their localization position as corner C, facet F, and corner facet CF modes, shown in (b). A second categorization can be made based on their singlet and duplet nature by looking at the phase of the wave along the azimuthal direction in (c); singlets are standing spin-wave solutions, while duplets are two degenerate solutions of counterpropagating waves along the azimuthal direction. In panels (d) and (e) the mode magnitude as well as its phase is shown for several examples of the singlet and duplet solutions. Below the modes, we annotate the corresponding irreducible representations (irreps) to which they belong.

to the ones in round nanotubes or rings in the vortex state where the azimuthal dependence of the mode profiles is given by  $\exp(im\phi)$  with  $m$  being an integer number often called the azimuthal mode index. In such cylindrical or tubular systems, modes with the same  $k$  but opposite sign of  $m$  are degenerate, i.e., they form duplets, except for the  $m = 0$  mode, which is a singlet. In the phase plots such as Fig. 3(c), loosely speaking, the number of periods is given by the number of times a color reappears as one goes along the circumference of the hexagonal cross section. As an important difference to the cylindrical systems, which are characterized by full rotational symmetry about the tube axis, the phase around the hexagonal cross sections does not increase linearly along the circumference. In fact, the discrete sixfold rotational symmetry induces

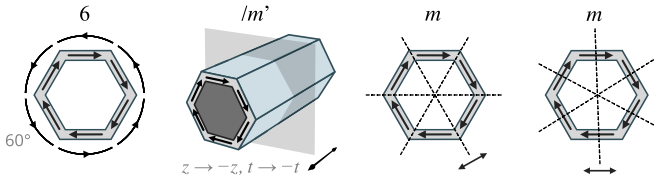


FIG. 4. Generators of the symmetry group  $6/m'mm$  shown for the hexagonal tube containing a vortex state, where 6 is the sixfold rotational symmetry,  $m$  indicate mirror planes and  $'$  is the time reversal operation.

drastic qualitative changes. We observe that, depending on the number of periods, the modes can be either doubly degenerate or nondegenerate, respectively forming duplets or singlets. Singlets form standing waves along the circumference, as can be seen in the  $\pi$  jumps of the phase of the C3 mode in Fig. 3(c). In contrast to this, the duplets consist of two solutions which have equal localization (magnitude) but are propagating in opposite directions along the circumference, as depicted for C2+ and C2− in Fig. 3(c). Albeit the phase does not increase in a linear fashion as in cylindrical systems, it still changes continuously. In Figs. 3(d) and 3(e), we show the mode profiles close to  $k = 0$  for all branches whose dispersion is plotted in Fig. 3(a). Notably, for all the modes the profile of the magnitude obeys the sixfold rotational symmetry of the hexagonal tube. The observed splitting of the spectrum into singlets and duplets has also been observed in a similar way for whispering gallery modes in hexagonal optical cavities [51].

In the following, we show how the splitting of some of the duplets to singlet pairs upon lowering the symmetry of the vortex tube from cylindrical to hexagonal can be understood via a basic group theory approach, even without considering the form of the magnetic interactions. The symmetry of the hexagonal vortex tube is described by the magnetic point group  $6/m'mm$ . The generators of the group are shown in Fig. 4: the sixfold rotational symmetry about the axis of the tube, two sets of mirror planes ( $m$ ) containing the axis of the tube, and the mirror plane perpendicular to the tube axis ( $/m'$ ). Due to the magnetic vortex pattern, the latter are symmetries only when combined with the time reversal operation ( $'$ ). This magnetic point group has only 1D and 2D irreducible representations; thus the excitations of the hexagonal magnetic vortex can form only singlets and duplets. No modes with triple or higher degeneracy can emerge. The singlet solutions listed in Fig. 3(d) can be classified according to the 1D representations of  $6/m'mm$  [52]. Since the amplitude map of all modes obeys all symmetries in this group, one needs to check how the phase pattern of the modes change upon the different symmetry operations. For singlets, the phase pattern can either be invariant upon a symmetry operation or acquire a  $\pi$  shift. The modes C0 and CF6 belong to the fully symmetric  $A_1$  irreducible representation, as their phase pattern is invariant upon all symmetry operations of the  $6/m'mm$  group. The phase pattern of the F6 mode is invariant upon all symmetry operation but the reflections to the mirror planes containing the tube axis; thus it belongs to the  $A_2$  irreducible representation. The classification is indicated for all the modes in Figs. 3(d) and 3(e). In the case of duplets, some of the

symmetry operations interrelate the phase patterns of the two modes, leading to a zero entry in the character table [52].

One can easily find a correspondence between the modes of the cylindrical and the hexagonal vortex. The C0 singlet corresponds to the only singlet mode of the cylindrical tube, which is nothing but the simple ferromagnetic resonance for  $k = 0$ . When the hexagonal symmetry is increased to cylindrical, the rest of the singlets become doubly degenerate, i.e., arrange into pairs, such as CF6-F6, C3-F3, etc. This is because modes localized to corners and facets become nondistinguishable once the cylindrical symmetry is restored.

We observe that modes with different periods around the circumference are hybridized, while it seems that singlets (duplets) hybridize only with singlets (duplets). In Fig. 3(a) the hybridization can be seen for the branches CF5 and CF7 and was confirmed by analyzing the mode profiles of the two branches on different sides of the crossings. To avoid visual clutter, we refrained from double labeling the branches twice. Let us also note that the dynamic-matrix approach used here can yield only the already hybridized normal modes of the system. Therefore, presenting a dispersion with the nonhybridized branches as well as a proper treatment of the hybridization would require an analytic theory, which is not available at the moment.

The same holds if one would like to disentangle the contributions resulting in the strongly asymmetric dispersion for some of the spin-wave modes. Based on our knowledge from the thin-shell cylindrical nanotubes we can state that the asymmetric dispersion has its origin in the dynamic charges associated with the dipole-dipole interaction. Let us note that the antiparallel alignment of the equilibrium magnetization in opposite facets would alone lead to an asymmetry, resulting in a linear shift of the dispersion in the small  $k$  limit [24]. However, in our case the asymmetry is far stronger than a linear shift and therefore suggests the presence of a geometrical volume charge due to the strongly curved regions between the flat facets. The concept of geometrical charges and its relation to possible magnetochiral effects are discussed in detail in Ref. [38]. A detailed discussion of the origin of the asymmetric dispersion as well as the presence of singlet and duplet states and their relation to the magnetic point group of our system is out of the purview of the current paper and will be investigated in a forthcoming work.

### C. Predicted microwave absorption and comparison with experiments

The dispersion branches excited in an experimental setup can drastically depend on the spatial distribution of the oscillating excitation field  $\mathbf{h}(\mathbf{r})$ , i.e., on the microwave antenna at hand. In the case of propagating waves, the microwave power absorbed by the magnetic system is determined by the overlap

$$h_v(k) = \frac{1}{\mathcal{N}_v} \langle \eta_{vk}^* \cdot \tilde{\mathbf{h}}(k) \rangle_A \quad (4)$$

with  $\tilde{\mathbf{h}}(k)$  denoting the Fourier transform of the spatial distribution of the microwave field with respect to the  $z$  coordinate (long axis of the tube),  $\langle \cdot \rangle_A$  denotes the spatial average in the hexagonal-tube cross section, and  $\mathcal{N}_v$  is a normalization factor (see Appendix A). The full frequency- and



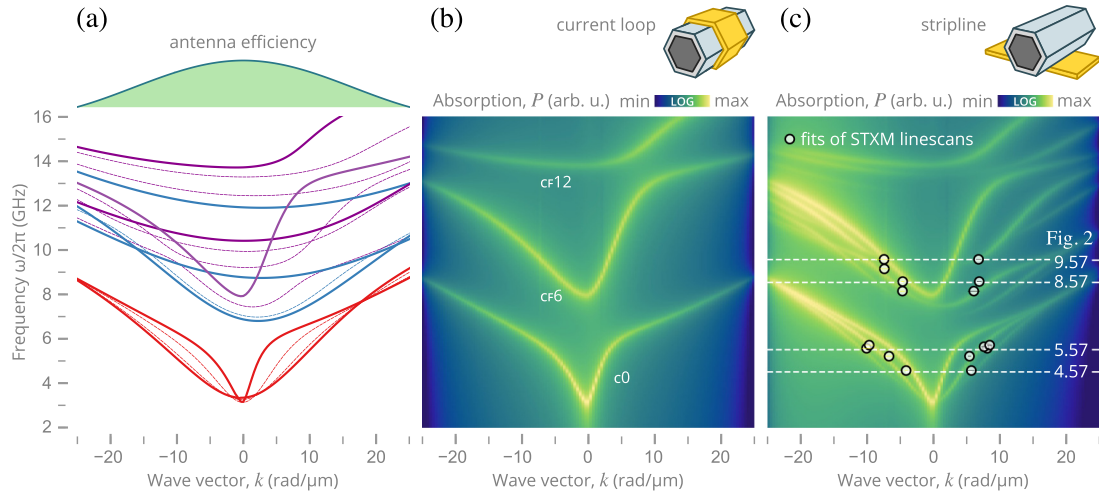


FIG. 5. Predicted microwave absorption calculated using the mode profiles from the dynamic-matrix approach for two different antenna geometries. (a) The zeroth-order peak of the excitation efficiency at the surface of the antennas is shown on the top of the full dispersion relation including all modes up to 16 GHz. The dispersion relation obtained when exciting spin-wave modes with a current loop antenna is shown in (b). Only singlets belonging to the fully symmetric  $A_1$  representation are susceptible to the spatial distribution of such a field. The dispersion relation for a stripline antenna used in the experiments is summarized in panel (c). The usual asymmetry of the excitation efficiency known for Damon-Eshbach modes is recovered. This antenna will excite simultaneously a multiple of modes with the same frequency. The white dashed lines indicate the excitation frequencies for which the experimental spatial spin-wave profiles are shown in Fig. 2.

wave-vector-dependent absorption is then given by summing up the response of all branches  $\nu$ , as

$$P(k, \omega) \propto \sum_{\nu} \frac{|h_{\nu}|^2(k)}{[\omega_{\nu}(k) - \omega]^2 + \Gamma_{\nu}^2(k)}. \quad (5)$$

Here  $\Gamma_{\nu} = \alpha_G \epsilon_{\nu} \omega_{\nu}$  is the life time of the spin-wave modes which is determined by the Gilbert damping factor  $\alpha_G$  and by the mode ellipticity  $\epsilon_{\nu}(k)$  (see Ref. [53] and again Appendix A).

In the following, we present the predicted absorption calculated for two different important antenna geometries: a single current loop wrapped around the nanotube and for a single stripline antenna attached to one of the facets, such as the one used in our experiments. We fix both antenna widths to  $W = 250$  nm. In Fig. 5(a) on top of the dispersion, we show the zeroth-order peak of the excitation efficiency at the surface of both antenna types, which is approximately given by  $|\text{sinc}(\Lambda k)|$ , with  $\Lambda \approx W/2$ . Exact expressions for the Fourier components of  $\vec{h}(k)$  for the presented antennas are found in Appendix B. As an important difference between the antenna geometries, the microwave field produced by a stripline antenna is inhomogeneous within the hexagonal cross section and is, therefore, not rotationally symmetric. While the microwave field produced by a current loop can be assumed to have a homogeneous magnitude along all facets. As a result, the spin-wave modes of particular symmetry propagating in the hexagonal tubes couple differently to the microwave excitation, depending on the specific field distribution. This knowledge is crucial when designing and interpreting experiments (and even classic time-domain micromagnetic simulations). To this end, in Fig. 5(b) we show the absorption  $P(k, \omega)$  for a current-loop microwave antenna. As can be seen, only a number of singlet branches (c0, c6, and c12) are susceptible to such a field. These are the only

modes which, according to their symmetry, exhibit a nonvanishing absorption in a rotationally symmetric microwave field in the observed frequency range. The period of these modes is an integer multiple of 6, and in general the period of the singlets is  $3n$ , with  $n \geq 0$ .

In contrast to this, the stripline antenna used in our experiments will couple to the singlet as well as to the duplet modes, as shown in Fig. 5(c). Note that the excitation efficiency of the spin-wave modes is asymmetric; therefore for the considered vortex state and antenna geometry the spin waves propagating with negative wave vector are excited stronger than the counterpropagating ones. As mentioned before, this is a commonly known effect for spin waves excited in the Damon-Eshbach geometry, namely,  $\vec{k} \perp \vec{m}_0$ , and is also seen when analyzing the individual frames of the spin-wave spatial profiles obtained from the TR-STXM experiments. The white dashed lines mark the excitation frequencies for which the experimental and micromagnetic simulation spatial profiles of the spin waves are presented in Fig. 2. The consequences of the stripline antenna microwave source are that multiple modes with the same frequency are excited simultaneously, leading to a beating pattern instead of a plane wave propagation pattern with a well-defined wave length. The presence of multiple wave lengths can already be seen when carefully looking at the propagating spin-wave profiles taken at given snapshots in time from the time-domain micromagnetic simulations presented in Fig. 2. Especially for the 4.571 GHz and 5.571 GHz frequencies it is quite obvious that multiple wave lengths are present. On one hand this explains why only certain frames from the experimental measurements could be used to approximately evaluate a wavelength for the excited spin waves. On the other hand, with this information in mind we need to emphasize that the determination of the wavelengths are rather imprecise. Still, without drawing conclusions, in Fig. 5(c) we have overlaid the experimentally determined



dispersion with the one yielded from the predicted microwave absorption using the spin-wave mode profiles of the dynamic-matrix approach simulations.

#### IV. CONCLUSIONS AND OUTLOOK

We have investigated spin-wave propagation in hexagonal nanotubes using time-resolved STXM measurements and micromagnetic simulations. The experimental results show that spin waves can be excited with a simple stripline antenna. Using a finite element dynamic-matrix approach for propagating spin waves, we calculated the dispersion relation for the hexagonal tube with geometrical and material parameters as in the experiments. The dispersion relation turned out to be asymmetric and complex. Due to the hexagonal cross section, spin waves can be localized to the highly curved corners, to the flat facets as well as to both sites at the same time. The hexagonal symmetry lifts the azimuthal mode degeneracy known from round nanotubes and results in singlet and duplet spin-wave solutions. The singlets are always standing spin-wave solutions, and their azimuthal mode index is an integer multiple of 3. The duplets consist of two degenerate spin-wave solutions counterpropagating along the azimuthal direction. We have shown that, using the spin-wave profiles resulting from the eigensolver, the frequency- and wave-vector-dependent microwave absorption of different antenna field profiles can be calculated. These numerical results show that the stripline antenna used in the TR-STXM experiments will simultaneously excite modes with the same frequency but different wave vectors. Therefore, the resulting spatial profile of the spin waves propagating in the nanotube forms a beating pattern instead of a single wave solution with a well-defined wavelength. These experimental results are not suitable for drawing conclusions about the spin-wave dispersion asymmetry that is present in the dispersion calculated by micromagnetic simulations, in either the time or frequency domain. We can conclude that the antenna design in further experiments needs to be changed, and if possible a single current loop should be used to allow for the excitation of single modes with a well-defined wave length. Alternatively one could use a CPW antenna which selectively excites spin waves with specific wave vectors. We hope that with the recent developments in materials research and fabrication methods the production of high-quality 3D nanostructures and waveguides (magnetic for this purpose) will be standardized and the investigation of exciting effects as the curvature-induced magnetochiral effects on the magnetization statics and dynamics will become feasible.

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#### APPENDIX A: MICROWAVE ABSORPTION AND LINE WIDTHS

Here we briefly describe how the microwave absorption is calculated from the lateral mode profiles  $\eta_{vk}$  obtained with our propagating-wave dynamic-matrix approach. As mentioned in the main text, the microwave power absorbed by the spin-wave system is determined by the overlap of the spin-wave mode profile with the spatial profile of the microwave field. Our formalism here is a special case of the general cases, e.g., discussed in Refs. [54] and [53]. For a general volumetric spin-wave mode profile  $\mathbf{m}_v(\mathbf{r})$  denoted only with the mode index  $v$ , the microwave absorption is obtained as

$$h_v = \frac{1}{\mathcal{M}_v V} \int_V dV' \mathbf{m}_v^*(\mathbf{r}') \cdot \mathbf{h}(\mathbf{r}'), \quad (\text{A1})$$

with  $V$  being the volume of the magnetic specimen,  $\mathbf{h}$  being the spatial profile of the microwave field, and  $\mathcal{M}_v$  being the normalization factor of the mode with respect to the volume, which is given by

$$\mathcal{M}_v = \frac{i}{V} \int_V dV' \mathbf{m}_v^*(\mathbf{r}') \cdot [\mathbf{m}_0(\mathbf{r}') \times \mathbf{m}_v(\mathbf{r}')]. \quad (\text{A2})$$

In our case, the mode profiles are given as  $\mathbf{m}_v(\mathbf{r}) = \eta_{vk} \exp(ikz)$  and the equilibrium magnetization is translationally invariant along the  $z$  direction,  $\mathbf{m}_0(\mathbf{r}) = \mathbf{m}_0(\boldsymbol{\rho})$ . For a very long waveguide with finite length  $L$ , one can now insert these mode profiles into Eqs. (A1) and (A2), perform the integral along the  $z$ -direction, and then let  $L \rightarrow \infty$ . One then obtains the wave-vector dependent overlap

$$h_v(k) = \frac{1}{\mathcal{N}_{vk} A} \int_A dA' \eta_{vk}^*(\boldsymbol{\rho}') \cdot \tilde{\mathbf{h}}(\boldsymbol{\rho}', k) \quad (\text{A3})$$

with  $\tilde{\mathbf{h}}(\boldsymbol{\rho}, k)$  being the Fourier transform of the microwave field along the  $z$  direction and  $\mathcal{N}_{vk} = \mathcal{M}_{vk}/L$  being the normalization factor of the mode with respect to the cross section area  $A$ , which is given as

$$\mathcal{N}_{vk} = \frac{1}{A} \int_A dA' \eta_{vk}^*(\boldsymbol{\rho}') \cdot [\mathbf{m}_0(\boldsymbol{\rho}') \times \eta_{vk}(\boldsymbol{\rho}')]. \quad (\text{A4})$$

In order to obtain the full microwave absorption, one also needs to know the line widths of the modes,  $\Gamma_{vk} = \alpha_G \epsilon_{vk} \omega_{vk}$ , which depend on the Gilbert damping parameter  $\alpha_G$  and the mode ellipticity  $\epsilon_{vk}$ . A general formalism to obtain the linear spin-wave damping from the mode ellipticities was presented in Ref. [53], which can be applied to our case in the same way as above. For our case we obtain

$$\epsilon_{vk} = \frac{1}{\mathcal{N}_{vk} A} \int_A dA' |\eta_v(\boldsymbol{\rho}')|^2. \quad (\text{A5})$$

## APPENDIX B: EXPRESSIONS FOR MICROWAVE-FIELD WAVE-VECTOR SPECTRA

In our specific study, we calculated the microwave absorption for a current-loop antenna around and a stripline antenna attached to the hexagonal nanotube. In the case of a current loop the wave-vector spectrum of the microwave field can be approximated as

$$\tilde{\mathbf{h}}^{(\text{loop})} \approx (\mathbf{e}_\xi(\boldsymbol{\rho}) + \mathbf{e}_z) |\text{sinc}(\Lambda k)| e^{-\beta_0 k} \quad (\text{B1})$$

with  $\Lambda \approx 125$  nm being approximately equal to half of the width of the antenna and  $\beta_0 = 0.5$  nm/rad being some decay factor. The unit vector field  $\mathbf{e}_\xi$  can be approximated as being the one locally perpendicular to both  $\mathbf{m}_0$  and  $\mathbf{e}_z$ , which, in the case of a hexagonal vortex state, gives the “radial” direction.

In the case of a stripline antenna which is attached to the facets of the hexagonal tube (without any loss of generality a facet which is parallel to the  $xz$  plane) the wave-vector spectrum can be approximated as

$$\tilde{\mathbf{h}}^{(\text{strip})} \approx (\mathbf{e}_x + \mathbf{e}_z) |\text{sinc}(\Lambda k)| e^{-\beta(s)k}. \quad (\text{B2})$$

Here  $\beta(s)$  is now a function which depends on the distance  $s$  to the center plane of the antenna. To obtain this dependence we calculated the full 3D profile of the stripline antenna and performed a Fourier transform in the  $z$  direction for different distances from the antenna. A simple linear approach gave a reasonable fit  $\beta(s) = \beta_1 s + \beta_0$  with  $\beta_1 \approx 1$  and again  $\beta_0 = 0.5$  nm/rad.

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